





Phil WATSON

The University of Western Australia and Chair of TC 209

The Role of Physical Modelling in Offshore Geotechnics

<u>Agenda</u>

- 1. What are we trying to achieve?
- 2. Types of physical modelling
- 3. There's a community out there!
- 4. Centrifuge modelling
- 5. Examples
- 6. Closing comments

What are we trying to achieve with physical modelling?

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Are we ...

- Prototyping new concepts?
- Studying mechanisms / behaviours?
- Assessing performance?
- Validating design?
- Calibrating of numerical models?
- Understanding risk?

... all of the above!

Other examples of physical modelling

Wind tunnel *Aerodynamics*

Tank testing Hydrodynamics





Physical modelling for geotechnical problems

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http://www2.eng.ox.ac.uk/geotech/research/PISA/FieldTests



Andersen, K.H. Bearing capacity under cyclic loading — offshore, along the coast, and on land. The 21st Bjerrum Lecture presented in Oslo, 23 November 2007. © Canadian Science Publishing or its licensors

Field scale testing

Investigate behavior at 'real' scale

Challenges:

- Large loads
- Matching ground conditions
- Cost (and schedule)

Small scale testing

Explore foundation systems

Challenges:

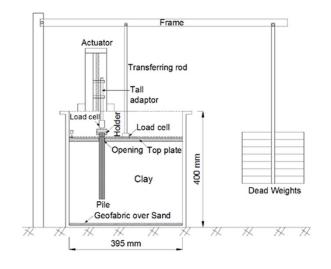
- Idealised model
- Soil conditions
- Stress conditions

Physical modelling for geotechnical problems

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Calibration chamber testing

Testing in uniform soil conditions

Challenges:

- Axial loading only
- Element response



Centrifuge testing

Explore foundation systems

Challenges:

- Idealised model
- Idealised soil



Focus for remainder of presentation

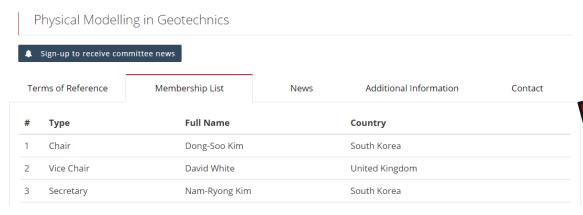
There's a community out there!

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ISSMGE TC104 'Physical Modelling in Geotechnics'



Honour lecture: Schofield Lecture

International journal and conference series



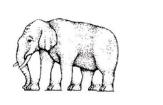
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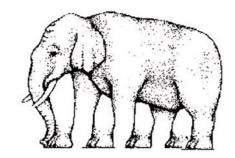


Start by looking at scale modelling, and think about an elephant ...

By how much can I multiply the size of an elephant before it collapses, unable to support it's own weight?

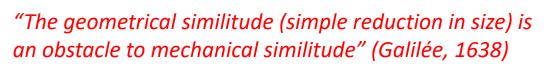






If the size is multiplied by n ...

- The cross section of bone's leg is multiply by n²
- The weight is multiply by n³





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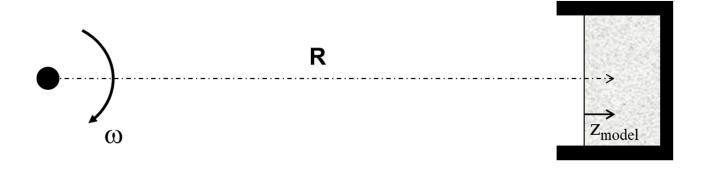


So if we want to scale our model, how do we address the issue raised by Galilée?

We can either ...

- Modify the mechanical properties of the materials; or
- Modify the values of the body forces

Centrifuge modelling achieves the latter



Acceleration = $\omega^2 R$ = ng $z_{model}/z_{prototype} = 1/n$ $\sigma_{model}/\sigma_{prototype} = 1$ (stress similitude)

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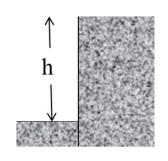


Why is stress similitude important for geotechnical engineers?

Stress governs both the applied forces and the behavior of the soil

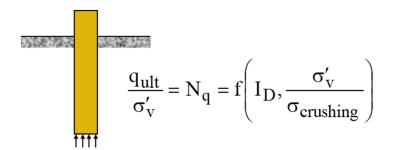
If not matched, then results will not be realistic

Clays (e.g. stability of vertical cut)

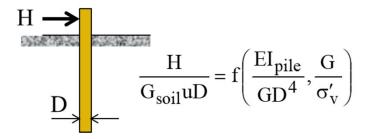


$$\frac{\gamma h}{s_u} = \frac{\sigma_v}{s_u} = N_s$$

Sands (e.g. end-bearing resistance)



Soil-structure interaction (e.g. lateral pile response)



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Common scaling factors for centrifuge modelling

PHYSICAL PARAMETER	SCALE FACTOR
Stress	1
Density	1
Acceleration	n
Length	1/n
Displacement	1/n
Strain	1
Velocity	1
Force	1/n²
Time, dynamic problems	1/n
Time, diffusion problems	1/n²

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There are many facilities around the world



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National Geotechnical Centrifuge Facility at The University of Western Australia





1.2 m diameter drum centrifuge



3.6 m diameter fixed beam centrifuge



10 m diameter fixed beam centrifuge

Examples – Soil characterisation

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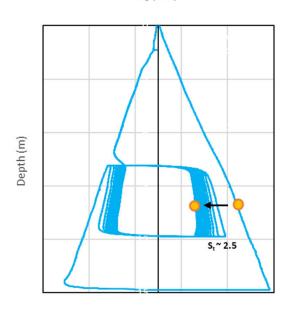




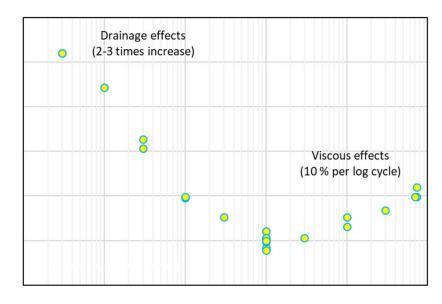
Development of new tools (e.g. T-bar)
Investigation of soil behaviour (e.g. rate effects)



s_u (kPa)



k/k_{ref}





Rate (model scale), mm/s

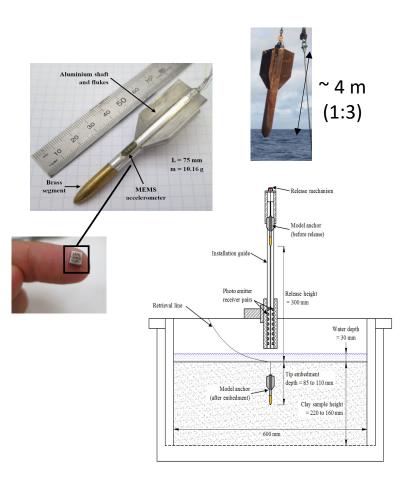
Examples – Prototyping

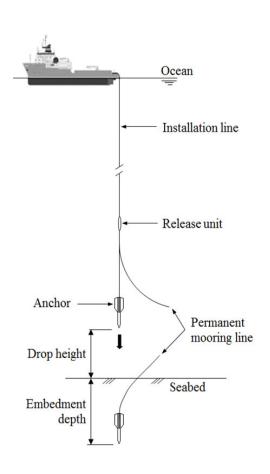
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Dynamically embedded anchors





Extreme strain rate effects
Water entrainment
Drag resistance in soil

Figure removed

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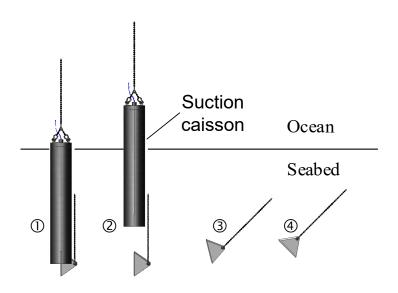


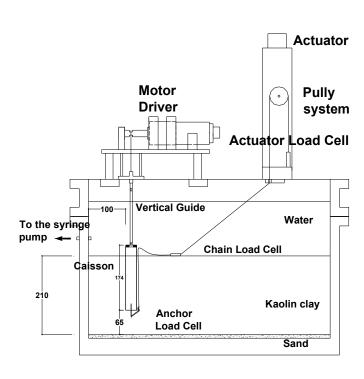


Suction embedded plate anchors







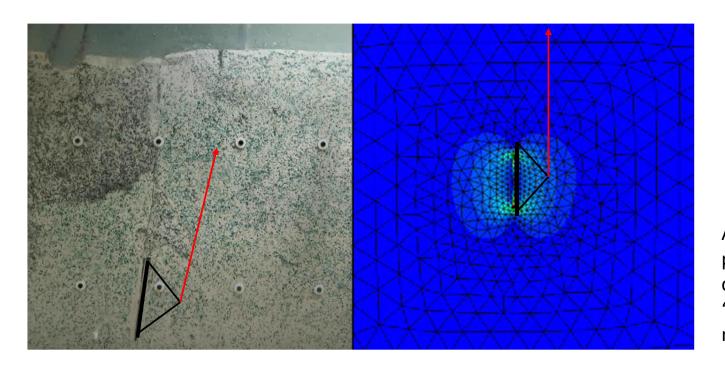


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Suction embedded plate anchors



Also highlights how physical modelling can be used to 'calibrate' numerical models

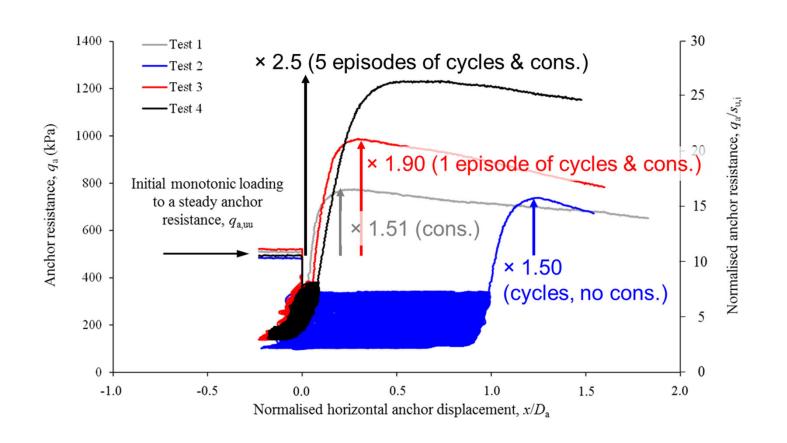
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Zhou, Z. O'Loughlin, C.D., White, D.J. Stanier, S. A. (2019) Improvements in plate anchor capacity due to cyclic and maintained loads combined with consolidation, Géotechnique, in press

Suction embedded plate anchors



Cycle back to prototyping (DEPLA)



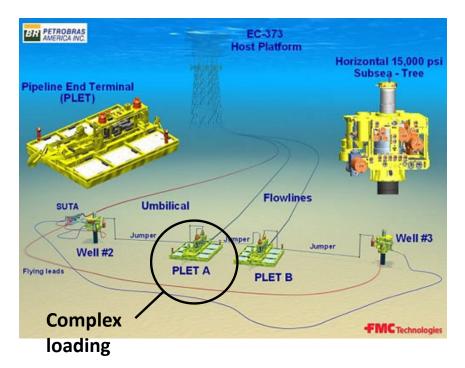
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Gaudin C., Randolph M.F., Clukey E., Dimmock P. (2012). Centrifuge modelling of a hybrid subsea foundation for subsea equipment. Proceedings of the 7th International Conference of Offshore Site Investigations and Geotechnics, London, England, 411-420.

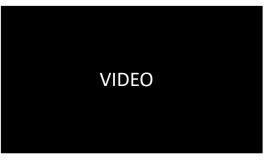
Hybrid foundations



Piles installed in flight V, Hx, Hy, Mx, My and Mz load



Figure removed



Examples – Soil-structure interaction

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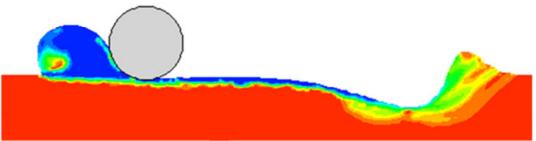


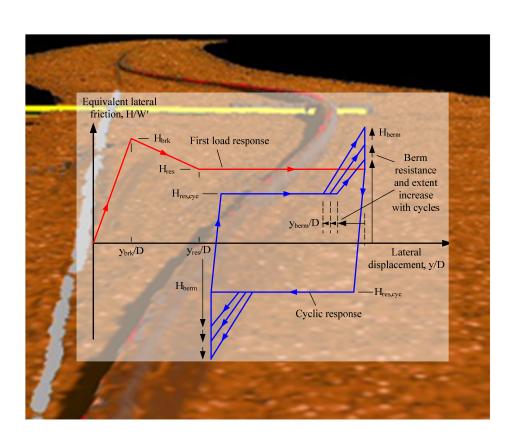


Behaviour of subsea pipelines

Soil response highly non-linear – needs to be captured for pipeline design (fatigue, stress)







Examples – Planning for installation

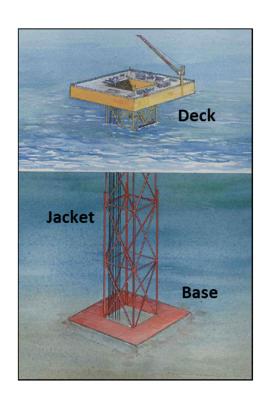
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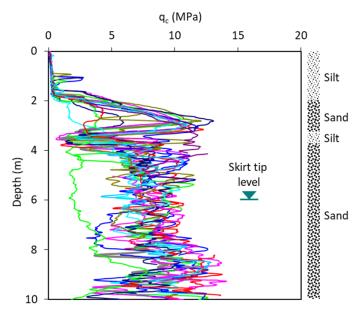




Watson, P.G., Jackson, G. & Humpheson, C. 2019. The Maari WHP foundation – Design, installation and performance, 13th Australia New Zealand Conference on Geomechanics, Perth, Australia

Suction installation in complex soils







Questions to be addressed:

- Would the silt layer lift during installation?
- Will seepage lower skirt resistance?

Examples – Planning for installation

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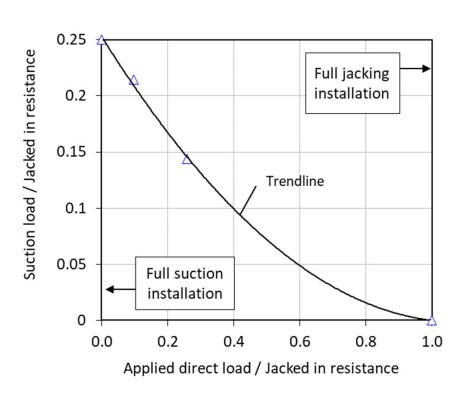
Watson, P.G., Jackson, G. & Humpheson, C. 2019. The Maari WHP foundation – Design, installation and performance, 13th Australia New Zealand Conference on Geomechanics, Perth, Australia

Suction installation in complex soils



Findings:

- Limited plug heave (full skirt installation)
- Suction reduces penetration resistance



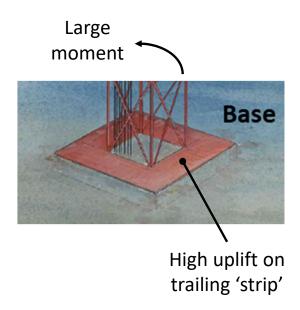
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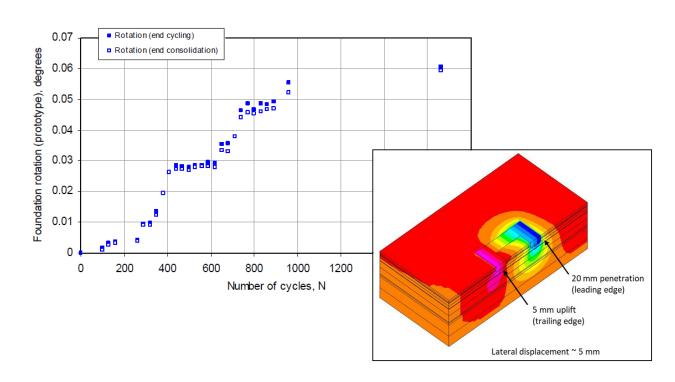


Watson, P.G., Jackson, G. & Humpheson, C. 2019. The Maari WHP foundation – Design, installation and performance, 13th Australia New Zealand Conference on Geomechanics, Perth, Australia

Foundation response under uplift loading







Currently testing uplift of caissons to support OWF jackets

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S_u (kPa)



Axial capacity of jetted conductors

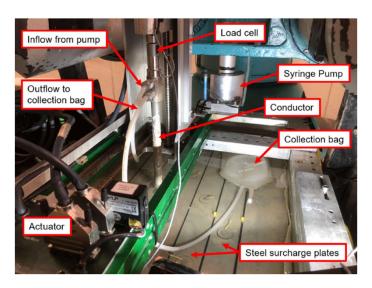
Jetting conductors

- Quick and cost effective
- Well suited to deep water



Issues

- Axial capacity uncertainty
- Subsidence (slumping) events

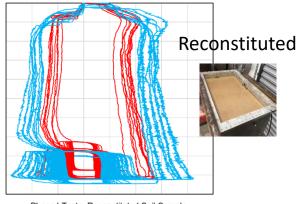




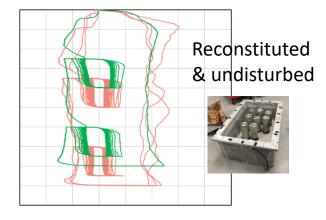
Testing explored:

- Capacity changes with time
- Broaching, collars, reciprocation (etc)





Phase I Tests, Reconstituted Soil Sample S_u (kPa)



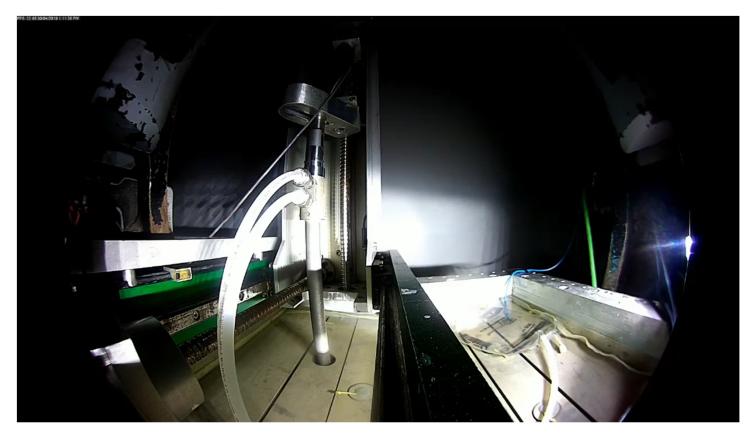
Challenges of Offshore Geotechnical Engineering Bodrum, Turkey - September 2019

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Axial capacity of jetted conductors

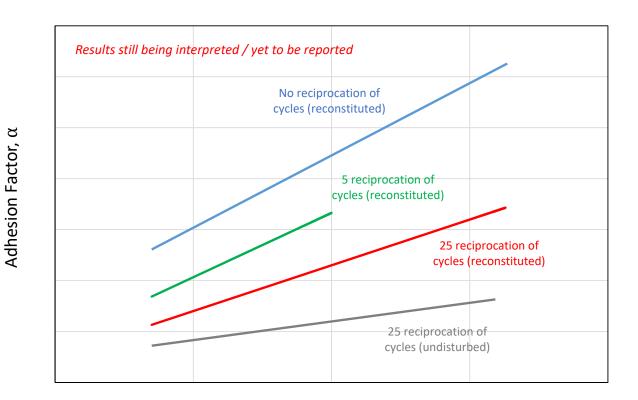


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Axial capacity of jetted conductors



Time (prototype days)

Capacity increases with time (setup)

Higher capacity for less 'damage' during installation

Undisturbed does not show same recovery with time

Results highlight an important consideration – capturing the behavior of soils with fabric (e.g. carbonate soils)

Closing comments

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Centrifuge modelling can be a valuable tool for an offshore engineer – I hope I have convinced you!

Like all tools – it needs careful consideration - and is (often) best used in combination with analytical/numerical tools, and good judgement!

ISFOG 2020 (an ISSMGE TC209 supported event) will be held in Austin, Texas

- This will include a prediction event participants asked to predict responses seen in the centrifuge
- Will also host the 5th McClelland Lecture to be delivered by Ed Clukey on the topic of physical modelling in geotechnics

Finally, I'd like to acknowledge my colleagues from UWA and beyond (especially Christophe Gaudin, Conleth O'Loughlin, Dave White, Alex Osuchowski)