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Rectangular raft of any rigidity on the layer of limited thickness

Radier rectangulaire de rigidité finie sur une couche d'épaisseur limitée

D.M. Milovic – Institute IMS, Belgrade, Yugoslavia

M.B. Djogo – Faculty of Technical Sciences, Novi Sad, Yugoslavia

ABSTRACT: The behaviour of rectangular raft of any rigidity resting on a homogeneous elastic layer of finite thickness is analyzed. The raft foundation is assumed to be uniformly loaded over the entire surface and, alternatively, over only a part of the foundation. The theoretical solution for determination of settlements w , bending moments M_x and M_y , torque M_{xy} , shearing forces N_x and N_y and reactive stresses q in any nodal point of a rectangular foundation of any rigidity is obtained by finite difference method.

RESUME: Cet article présente l'étude du comportement de la fondation rectangulaire de rigidité finie reposant sur un sol homogène et élastique d'épaisseur limitée. On a supposé que la fondation est sollicitée par une charge uniformément répartie ou, alternativement, par une charge partielle. La solution théorique pour la détermination des tassements w , moments de flexion M_x et M_y , moments de torsion M_{xy} , forces de cisaillement N_x et N_y et pressions de contact q pour chaque point nodal de la fondation a été obtenu par la méthode de différence finie.

1 INTRODUCTION

The contact problem of a rectangular raft foundation has been studied by several authors. Ueshita and Meyerhof (1968) and Milovic and Tournier (1971) have presented solutions for stresses and settlements produced by a uniformly loaded rectangular area. Brown and Gibson (1979) have given the solution for surface settlement of a rectangular foundation, resting on an elastic material, whose Young's modulus increases linearly with depth. For an elastic layer of finite thickness overlying a rough incompressible base Milovic and Tournier (1973), Fraser and Wardle (1976), Dempsey and Li (1989) have presented some results for contact stresses and settlements produced by symmetric loading over a rectangular rigid raft foundation.

This Paper shows solutions for determination of settlements w , bending moments M_x and M_y , torque M_{xy} , shearing forces N_x and N_y and reactive stresses q in any point of a square or rectangular raft foundation. For soil model an elastic and isotropic half-space was assumed, whereas the raft foundation can be of any rigidity. The solutions have been obtained by the finite difference method.

2 THEORETICAL ANALYSIS

The square or rectangular plate was divided by parallel lines in x and y directions into a grid system with a size of λ_x and λ_y , as shown in Figure 1.

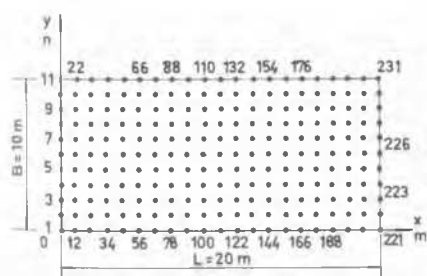


Figure 1. Finite difference grid system

The deflection of the foundation plate loaded by $p(x,y)$ is defined by the partial differential equation:

$$\frac{\partial^4 w}{\partial x^4} + 2 \cdot \frac{\partial^4 w}{\partial x^2 \partial y^2} + \frac{\partial^4 w}{\partial y^4} = \frac{p(x,y) - q(x,y)}{D} \quad (1)$$

where $w = w(x,y)$ unknown function of the vertical displacement of the central part of the slab, q = unknown function of the reactive stresses. The flexural rigidity of the plate is given by:

$$D = \frac{E \cdot h^3}{12 \cdot (1 - \mu^2)} \quad (2)$$

where h is the thickness of the plate.

The system of linear algebraic equations is given in the following matrix form:

$$[A] \cdot \{w\} = \frac{\lambda_x^4}{r^2 \cdot D} \cdot [\{p\} - \{q\}] \quad (3)$$

where $[A]$ = matrix of coefficients in the system of linear algebraic equations, $\{w\}$ = one dimensional matrix for vertical displacements, $\{p\}$ = one dimensional matrix for the applied load which acts in nodal points, $\{q\}$ = one dimensional matrix for the reactive stress which acts in nodal points. The relationship between the unknown vectors $\{w\}$ and $\{q\}$ can be expressed in the following matrix form:

$$\{w\} = [F] \cdot \{q\} \quad (4)$$

where $[F]$ = square matrix for the settlement of a point of the plate.

Using the expression (4) it is possible to determine the reactive stresses q and settlements w of all points on the plate, and after that the shear forces N_x and N_y , the bending moments M_x and M_y and the torque M_{xy} . Shearing forces and moments can be calculated by the expressions:

$$M_x = -D \cdot \left(\frac{\partial^2 w}{\partial x^2} + \mu \cdot \frac{\partial^2 w}{\partial y^2} \right) \quad (5)$$

$$M_y = -D \cdot \left(\frac{\partial^2 w}{\partial y^2} + \mu \cdot \frac{\partial^2 w}{\partial x^2} \right) \quad (6)$$

$$M_{xy} = -D \cdot (1 - \mu) \cdot \frac{\partial^2 w}{\partial x \partial y} \quad (7)$$

$$N_x = -D \cdot \left(\frac{\partial^3 w}{\partial x^3} + \mu \cdot \frac{\partial^3 w}{\partial x \partial y^2} \right) \quad (8)$$

$$N_y = -D \cdot \left(\frac{\partial^3 w}{\partial y^3} + \mu \cdot \frac{\partial^3 w}{\partial y \partial x^2} \right) \quad (9)$$

3 RESULTS

On the basis of the obtained theoretical solution the values of w , q , M_x , M_y , M_{xy} , N_x and N_y have been calculated for several values of the L/B ratio (where L is the length and B is the width of the foundation), for various relative stiffnesses K of the foundation raft and for a few values of the Poisson's ratio of soil μ .

The relative stiffness of the plate is defined by the expression (Fraser and Wardle 1976):

$$K = \frac{4 \cdot E_b \cdot (1 - \mu_s^2) \cdot h^3}{3 \cdot E_s \cdot (1 - \mu_b^2) \cdot B^3} \quad (10)$$

where E_b , E_s = modulus of elasticity of the raft and the soil, respectively; μ_b , μ_s = Poisson's ratio of the raft and the soil, respectively; h = thickness of the raft; B = width of the raft.

Some of the obtained results are shown in terms of dimensionless coefficients. So, the coefficients I_w for the settlement calculation of the corner and the center of a raft are shown in Figure 2. These coefficients are given for various values of H/B (where H is the thickness of a compressible layer), and for several values of K . The coefficients I_w for the partly loaded raft foundation are shown in Figure 3.

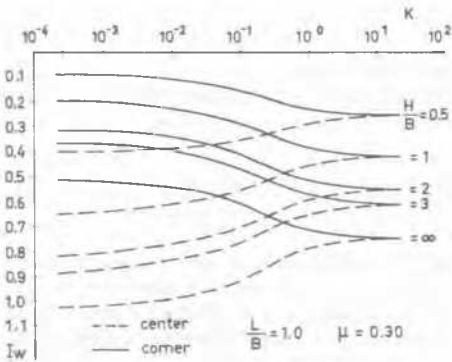


Figure 2. Coefficients I_w ; uniform load

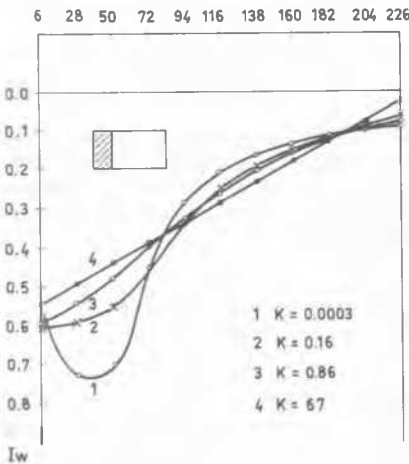


Figure 3. Coefficients I_w ; partly loaded raft

The coefficients I_{Mx} for the calculation of bending moments M_x , produced by partly loaded raft are shown in Figure 4.

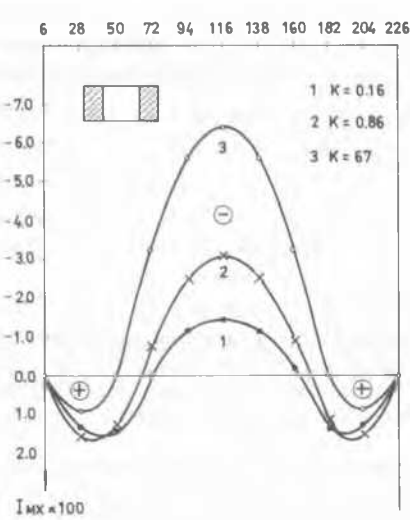


Figure 4. Coefficients I_{Mx} ; partly loaded raft

The curves shown in the above Figures represent only a few examples of the obtained results. As a matter of fact, on the basis of the obtained solution it is possible to obtain for any nodal point of the raft the values of w , q , M_x , M_y , M_{xy} , N_x and N_y , for any value of the ratio H/B and for any stiffness K of the raft.

4 CONCLUSIONS

1. Relative stiffness of the slab foundation has considerable influence on values of settlements, reactive stresses, moments and shearing forces and must be involved in design of a raft foundation.
2. The thickness of the compressible layer has a significant influence on the values of settlements and moments.
3. The degree of precision of the results obtained by finite difference method becomes higher with the finer grid.

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