

# INTERNATIONAL SOCIETY FOR SOIL MECHANICS AND GEOTECHNICAL ENGINEERING



*This paper was downloaded from the Online Library of the International Society for Soil Mechanics and Geotechnical Engineering (ISSMGE). The library is available here:*

<https://www.issmge.org/publications/online-library>

*This is an open-access database that archives thousands of papers published under the Auspices of the ISSMGE and maintained by the Innovation and Development Committee of ISSMGE.*

# Tensile Behaviour of Compacted Clays by Field Test

## Essais de Fissuration "In Situ" des Sols Compactés

S. URIEL ROMERO

Dr. Ing. C.C., y P., Head Soil Mechanics Department, Laboratorio de Carreteras y Geotecnia, Madrid, España

J.R. PÉREZ RODRIGUEZ

Dr. Ing. C.C., C.C. y P. Laboratorio de Carreteras y Geotecnia, Madrid, España

**SUMMARY** A field test for the investigation of the deformability conditions of a compacted soil under a tensile stress field is presented. It overcomes the inconvenients of laboratory tests. It is very interesting in order to study the appearance of cracks in earth or earth-rock dams, very frequently observed near the crest.

### 1. INTRODUCTION

The strenght and the deformability of saturad or unsaturad soils under a tensile stress field, is a very interesting problem, in relation with some earth works. The cracking of high earth embankments and specially the cracking of earth or rock-fill dams with clay core, is a problem which calls the attention of the design and construction civil engineer.

The investigation of such soil characteristics is made normally in a laboratory scale. The direct tensile test (Tschebotarioff, 1953), the deflection beam test (Ajaz and Parry, 1975), the point-load test (Fang and Chen, 1971), the Brazilian test (Gopala and Einsenstein, 1974), are the most commonly employed methods. These test are very usefull for establishing the influence of several parameters, like the soil type, the density and moisture content of the soil, etc., but they present some inconvenients when we intend to apply the results to foreseen the behaviour of real earth works. The main reasons, to the authors opinion, about the differences observed between calculated and observed movements before the cracking, are the following.

a) A great stress and strain gradient across the laboratory sample within very short distances, which has influence on the strenght of tensile zones.

b) In many cases, the laboratory experimentation is carried out on the finest fraction of the core material. The fraction above 3/4" or 1/2" is normally neglected, but its influence can be great on the results, if the percentage is greater than, say, 10 or 15%, depending on the type, of soil or particle size.

c) The structure of the soil in laboratory may be different than the "in situ" core material, due to the different method employed for the compaction.

The large scale investigations is restricted up to now to the analisis and interpretation of the observed cracking in earth embankments. The data obtained are not easily extrapolated to another cases due to the scarce and erratic measurements available in the stress-strain field before failure, or on the real conditions of the soil after the compaction (Leonards and Narain, 1963).

In this report a large scale "in situ" tests is presented. This test allows the investigation of the tensile behaviour of compacted soils, without the limitations above mentioned.

### 2. TEST DESCRIPTION

One experimental embankment, 8,5 m wide on its base and 2,5 m high compacted with the same soil and with the same machinery employed in the real works, is heaved by means of a special flat jack placed transversally across the base (Fig. 1). This jack is composed

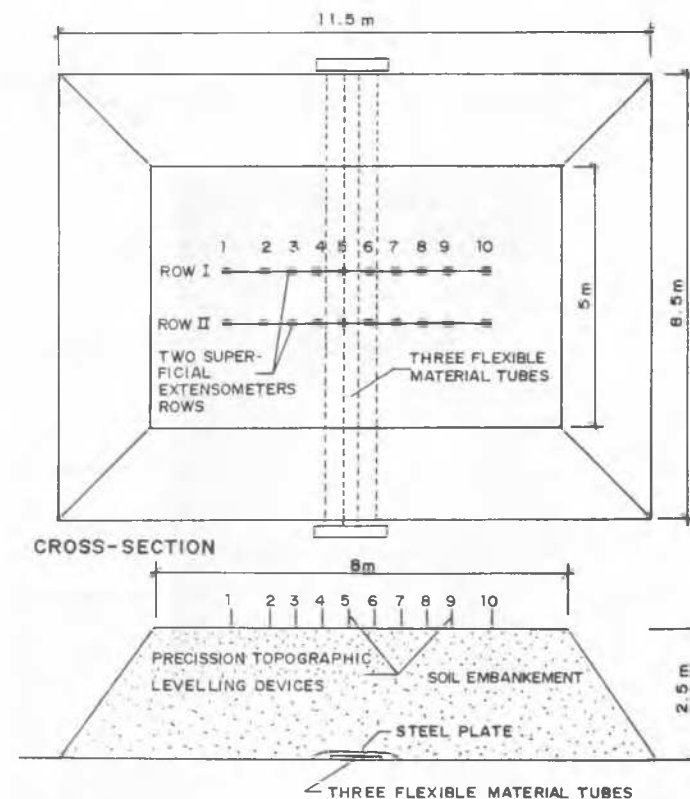


Fig. 1. - Experimental embankment lay out. Flat jack and extensometers situation

## 2. TEST DESCRIPTION

One experimental embankment, 8,5 m. wide on its base and 2,5 m. high, compacted with the same soil and with the same machinery employed in the real works is heaved by means of a special flat jack placed transversally across the base (fig. 1). This jack is composed by three flexible material tubes, 20 cm. diameter when inflated (fig. 2). The three tubes are protected between PVC



Fig. 2. - Hidraulic flat jack composed by three flexible material tubes

plates, and covered by mild steel plates, 3 mm. thick (fig. 3 and 4). These plates distribute the jack pressure



Fig. 3. - The flat jack covered by PVC. and steel plates



Fig. 4. - Embankment compaction on the flat jack

on the compacted clay embankment fill. The flexible hoses are put under pressure by water. The fill is pushed upwards until the tensile stress induced in the surface produce the cracking of the fill. The first fissure appearance is specially noted and observed.

The horizontal strains are measured between fixed points (fig. 1) by means of pirez rods and extensometer 1/100 mm. precision (fig. 5). The vertical movements are measured by means of levelling devices situated at the same reference points. Two rows of such points, 50 cm. apart, in the central zone of the fill, and 75 cm in the external zone are placed on the upper surface of the embankment (fig. 6)

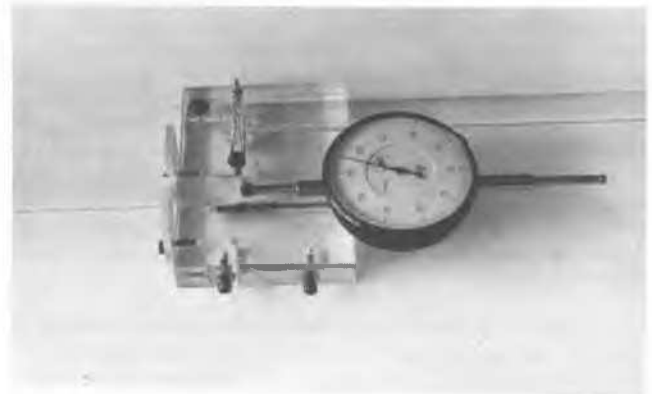


Fig. 5. - Extensometer device. The tensile strain is measured between fixed points, by means of pirez rods

In order to avoid moisture content losses during the preparation and performance of the test, the clay is covered with parafine oil. In addition a thin plaster powder is extended on the measuring zone for a better observation of the appearance of the cracking.



Fig. 6. - Two rows of extensometers for measuring tensile strain in the embankment surface.

3. TEST RESULTS

The first experimental fill was constructed at the Canales dam site, near Granada. It is under construction, - and when completed will be the highest rock fill dam in Spain (150 m.). The clay core is subvertical and thin.

The rock abutments have a slope 1 h: 3v, but the right one has an abrupt change in the upper third of dam height, to 2,5 h: 1 v. By these reasons the possibility of the - cracking of the crest is investigated by all the available methods.

The clay material, with which the core and the experimental fill is constructed, has the following mean characteristics:

- Liquid limit 65 %
- Plasticity index 40 %
- Dry density 1,65 T/m<sup>2</sup>
- Moisture content 19 %

This moisture content is about 3 - 4 % below Optimum Proctor.

The fill was compacted in layers 30 cm. thick with 6 passes of taper-foot type sheepsfoot roller, as it is the case at the dam site.

In figure 7, the vertical upward displacement of the embankment surface is plotted for different jack pressures; it can be observed the typical dome shape of the fill profile. In figure 8 the strains, either tensile or compressive, between each pair of reference points is plotted against the jack pressure.

The first crack appeared between points 5 and 6 for a - jack pressure of 3,4 kg/cm<sup>2</sup>. At this moment the unit tensile strain between such points was 0,24%. The maximum vertical displacement of the surface was about 19,2 m (point n<sup>o</sup> 7).

For a better interpretation of the test, it was analyzed by

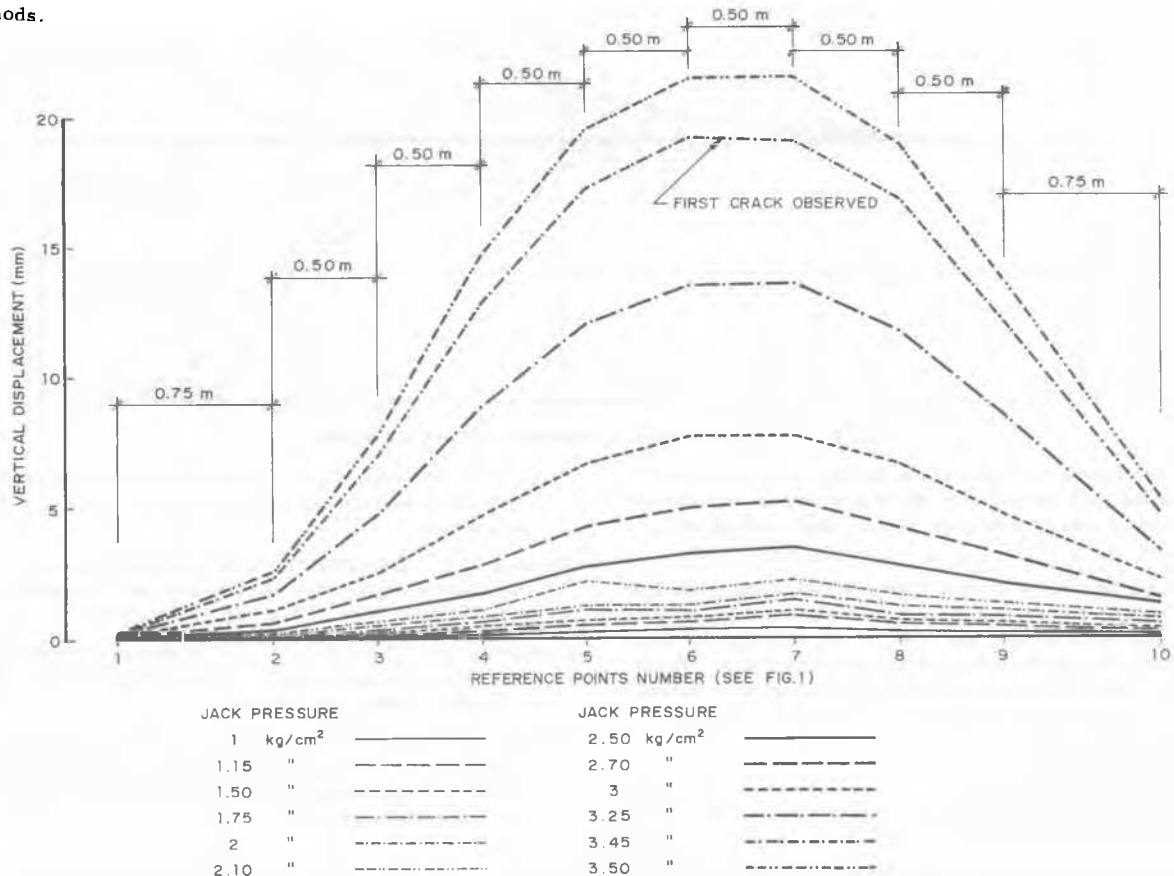


Fig. 7. - Vertical displacements of the reference points

the finite element method. The soil was supposed to be elastic, with a poisson ratio of 0,3, for compressive and tensile stress field.

From the comparison between calculated and observed movements, the following conclusions can be deducted:

19) Until a flat jack pressure of about  $2 \text{ kg/cm}^2$  the behaviour of the fill can be considered elastic, for tensile strain up to  $5 \times 10^{-4}$ , due to an almost linear relation between movements and pressure.

The mean elastic modulus within the tensile zone was in the range  $240\text{-}390 \text{ kg/cm}^2$ , and for the compressive zone, between  $130\text{-}300 \text{ kg/cm}^2$ .

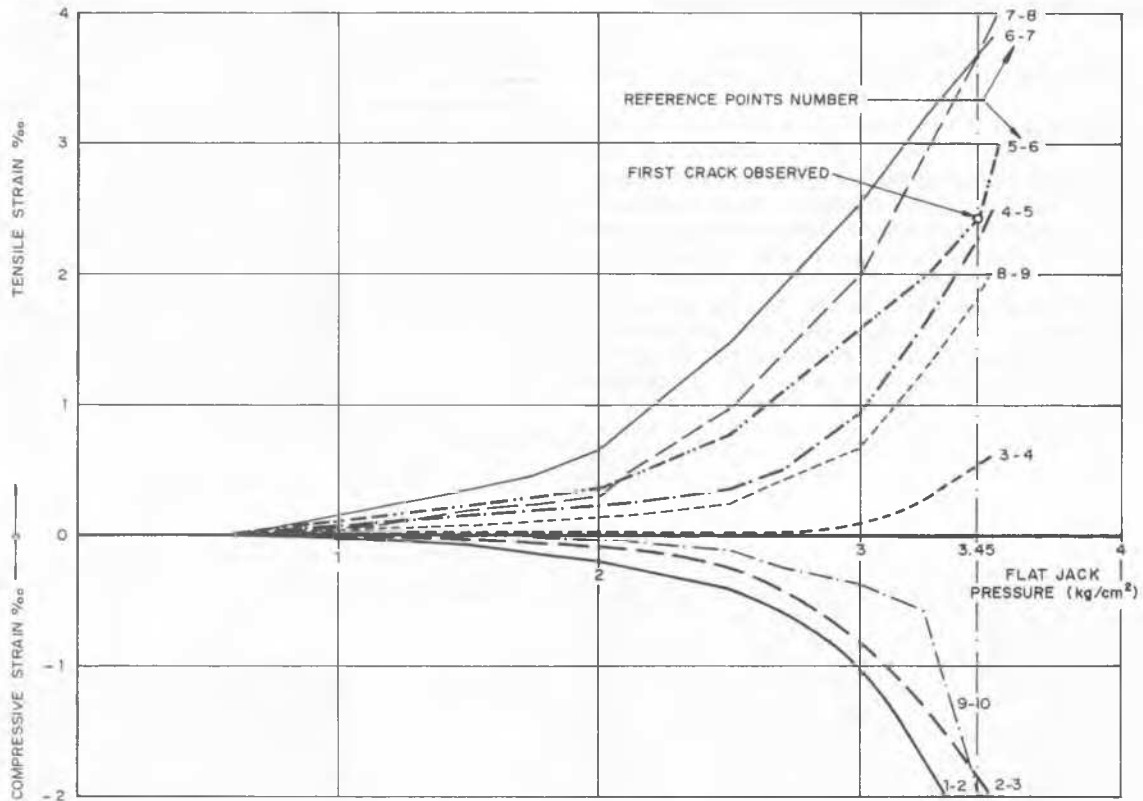


Fig. 8. - Horizontal strains between reference points

20) For greater values of the strain, the behaviour is not elastic, till the failure. When the first crack appeared, the mean elastic modulus in this zone was about  $120 \text{ kg/cm}^2$ .

30) The field tensile strain before cracking measured (0,24%) is situated among the values obtained in laboratory tests, but in this case the results were rather erratic, although the soil particles greater than  $3/4''$  were removed. That figure fits also well within the limits obtained with other clays compacted near the optimum proctor conditions (0,1-1%).

#### 4. FINAL REMARKS

The described field test is really a great scale flexo-traction test on a soil beam of 2,5 m thick.

The complete test duration was about nine hours. Nevertheless, if it is convenient to investigate the reological properties of the soil, the test duration can be enlarged

to several days, without difficulty. In the same way, it is well adapted to study the erodability of the soil, due to the filtration of water through a fissure. It is possible to investigate also the risk of piping, by reproducing together a zone of the core and filters. Both are fissured by the explained method. The percolation of water throught the cracks can be examined, and the autosealing or not of the fissure, studied.

#### REFERENCES

Ajaz, A. & Parry, R. G. H., "Stress-strain behaviour of two compacted clays in tension and compression", *Géotechnique*, XXV, 3, 1975, pp. 492-512.

Fang, H. Y. & Chen, W. F., "New method for determination of tensile strength of soils", H. R. B. 341, 1971, pp. 62-68.

Gopata, A. V., Einsenstein, Z. & Morgenstern, N. R., "Behaviour of compacted soil in tension" *Journal G. E. D.*, ASCE, 100, GT9, 1974, pp. 1051-1061.

Leonards, G. A. & Narain, J., "Flexibility of clay and cracking of earth dams", *Journal S. M. F. D.*, ASCE, 89, SM2, 1963, pp. 47-98.

Tschebotarioff, G. P., Ward, E. R. & Dephilippe, A. A., "The tensile strength of disturbed and recompacted soils", *Proceeding of the First Int. C. S. M. F. E.*, I Zurich, 1953, pp. 207-210.