# INTERNATIONAL SOCIETY FOR SOIL MECHANICS AND GEOTECHNICAL ENGINEERING



This paper was downloaded from the Online Library of the International Society for Soil Mechanics and Geotechnical Engineering (ISSMGE). The library is available here:

https://www.issmge.org/publications/online-library

This is an open-access database that archives thousands of papers published under the Auspices of the ISSMGE and maintained by the Innovation and Development Committee of ISSMGE.

# Calibration of Vs Prediction Model based on SPT-N using Conditional Probability Theory

#### T. Kishida

Pacific Earthquake Engineering Research Center, University of California, Berkeley, USA

C-C. Tsai

National Chung Hsing University, Taiwan

ABSTRACT: Prediction models of shear wave velocity  $(V_s)$  based on the standard penetration test (SPT) blow counts (N) are widely used in design practice. However, application of these models is limited because these models are typically ranged between regions. Moreover, it is difficult to calibrate the regression parameters for a site specific condition if multicollinearity exists in the model. This paper proposes a calibration procedure for developing a site specific  $V_s$  prediction model. The framework is based on conditional probability theory by developing correlations of model parameters from a global database. An application example is presented to develop the site specific  $V_s$  prediction model based on the available local N measurements. The framework of the conditional probability theory provides the rational approach to calibrate the site specific  $V_s$  prediction model.

#### 1 INTRODUCTION

Standard penetration test (SPT) blow count (N) is available at many sites throughout the world. On the other hand, shear wave velocities  $(V_s)$  are less available compared to N. Since  $V_s$  profiles are required for dynamic analysis and site characterization, the correlation of  $V_s$  and N is widely used for many design practice. Brandenberg et al. (2010) and Wair et al. (2012) summarized the previous studies and showed that most prediction models use the functional form of  $V_s = AN^B$ . Brandenberg et al. (2010) also presented multiple linear regression models for  $V_s$  by using N and effective overburden stress ( $\sigma'_{vo}$ ) as predictor variables, showing that it improves the prediction capabilities. However, it is recognized that  $V_s$  prediction models range widely between sites that is an importance issue to improve the prediction capability (Brandenberg et al. 2010 and Wair et al. 2012). Based on this reason, this paper proposed an approach to calibrate  $V_s$  prediction model for the site specific condition based on the conditional probability framework.

### 2 V<sub>S</sub> PREDICTION MODELS CONDITIONED ON N MEASUREMENTS

#### 2.1 Model Development

It is assumed that N is modeled with  $\sigma'_{vo}$  by a simple regression equation,

$$\ln N = b_0 + b_1 \ln \sigma_{vo}' + \varepsilon_N \tag{1}$$

where  $\varepsilon_N$  represents the residuals that follows normal distribution with standard deviation of  $\sigma_N$ . Similarly, it is assumed that  $V_s$  is modeled with  $\sigma'_{vo}$  by a simple regression equation,

$$\ln V_{s} = c_{o} + c_{1} \ln \sigma_{vo}' + \varepsilon_{vs} \tag{2}$$

where  $\varepsilon_{Vs}$  are residuals following normal distribution with standard deviation of  $\sigma_{Vs}$ . Correlation between  $\varepsilon_N$  and  $\varepsilon_{Vs}$  is also defined as  $\rho_{NVs}$  from Equations (1) and (2). Based on the conditional prediction of  $V_s$  given N measurement, the following formula is obtained.

$$E[\ln Vs \mid \ln N] = \beta_0 + \beta_1 \ln N + \beta_2 \ln \sigma'_{vo}$$
 (3)

where

$$\beta_0 = c_0 - b_0 \frac{\sigma_{Vs}}{\sigma_N} \rho_{NVs} \tag{4}$$

$$\beta_1 = \frac{\sigma_{V_S}}{\sigma_N} \rho_{NV_S} \tag{5}$$

$$\beta_2 = c_1 - b_1 \frac{\sigma_{Vs}}{\sigma_N} \rho_{NVs} \tag{6}$$

Standard deviation is calculated as;

$$\sigma_{V_S|N}^2 = \sigma_{V_S}^2 \left( 1 - \rho_{NV_S}^2 \right) \tag{7}$$

Equations (3) to (7) become the basis of conditional probability approach.

#### 2.2 Variation of Simple Regression Parameters

Database of  $V_s$  and N was developed from three data resources of Taiwan Strong Motion Instrument Program (TSMIP), Kyoshin Network (K-NET) by National Research Institute for Earth Science and Disaster Prevention and Oakland International Airport (OAK). Data from TSMIP and K-NET are available for public. The data for OAK was obtained from the previous study (Arulnathan et al. 2009). The database includes approximately 1,400 soil profiles. Effective stresses were computed for

each boring from the available unit weight and depth of water table. If the depth of water table is not available, it was determined when the P-wave velocity becomes 1,500 m/s. The N is corrected to  $N_{60}$  with the associated correction factors from past studies.

By running the simple regression analyses with Equations (1) and (2) for the developed database, Figure 1 was obtained. Mean, standard deviations, and correlations of these parameters are also presented in Equations (8) to (10).

## 2.3 Variation of $\beta_0$ , $\beta_1$ , $\beta_2$ and $\sigma_{VsN}$ for prediction model of Vs with N

Figure 2 shows the scatter plots of  $\beta_0$ ,  $\beta_1$ , and  $\beta_2$  for clay, silt and sand obtained from the aforementioned data sources. The figure shows that there is no clear difference in the distribution of the parameters among clay, silt and sand. This observation implies that regional factors such as geologic conditions contribute more to the variation of  $\beta_0$ ,  $\beta_1$ , and  $\beta_2$  more than soil type.

$$\hat{b}_0 \quad \hat{b}_1 \quad \hat{c}_0 \quad \hat{c}_1 \quad \hat{\sigma}_N \quad \hat{\sigma}_{V_S} \quad \hat{\rho}_{V_{SN}} = \begin{bmatrix} 0.484 & 0.489 & 4.21 & 0.251 & 0.840 & 0.322 & 0.400 \end{bmatrix}$$
 (8)

$$\begin{bmatrix} \sigma_{b0} & \sigma_{b1} & \sigma_{c0} & \sigma_{c1} & \sigma_{\sigma N} & \sigma_{\sigma V_S} & \sigma_{\rho V_S N} \end{bmatrix} = \begin{bmatrix} 1.97 & 0.436 & 0.763 & 0.163 & 0.212 & 0.115 & 0.276 \end{bmatrix}$$
 (9)

$$\begin{bmatrix} 1 & \rho_{b0b1} & \rho_{b0c0} & \rho_{b0c0} & \rho_{b0c1} & \rho_{b0aN} & \rho_{b0aV} & \rho_{b0\rho VSN} \\ \rho_{b0b1} & 1 & \rho_{b1c0} & \rho_{b1c1} & \rho_{b1cN} & \rho_{b1aN} & \rho_{b1aVS} & \rho_{b1\rho VSN} \\ \rho_{b0c0} & \rho_{b1c0} & 1 & \rho_{c0c1} & \rho_{c0aN} & \rho_{c0aVS} & \rho_{c0\rho VSN} \\ \rho_{b0c1} & \rho_{b1c1} & \rho_{c0c1} & 1 & \rho_{c1aN} & \rho_{c1aVS} & \rho_{c1\rho VSN} \\ \rho_{b0aN} & \rho_{b1aN} & \rho_{c0aN} & \rho_{c1aN} & 1 & \rho_{aNaVS} & \rho_{aVS\rho VSN} \\ \rho_{b0aVS} & \rho_{b1aVS} & \rho_{b1aVS} & \rho_{c0aVS} & \rho_{c1aVS} & \rho_{aNaVS} & 1 & \rho_{aN\rho VSN} \\ \rho_{b0\rho VSN} & \rho_{b1\rho VSN} & \rho_{c0\rho VSN} & \rho_{c1\rho VSN} & \rho_{aN\rho VSN} & 1 \end{bmatrix} = \begin{bmatrix} 1 & -0.955 & 0.414 & -0.394 & 0 & 0 & 0 \\ -0.955 & 1 & -0.402 & 0.455 & 0 & 0 & 0 \\ 0.414 & -0.402 & 1 & -0.938 & 0 & 0 & 0 \\ 0.414 & -0.402 & 1 & -0.938 & 0 & 0 & 0 \\ -0.394 & 0.455 & -0.938 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0.373 & 0 \\ 0 & 0 & 0 & 0 & 0.373 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

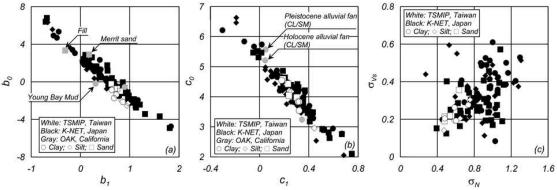


Figure 1. Variation of  $b_0$ ,  $b_1$ ,  $c_0$ ,  $c_1$ ,  $\sigma_{vs}$ , and  $\sigma_N$  for clay, silt, and sand

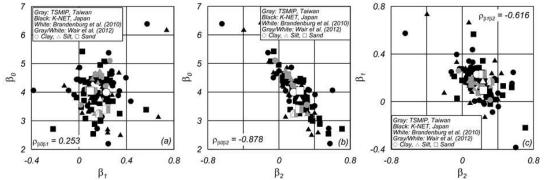


Figure 2. Variations of (a)  $\beta_0$  and  $\beta_1$ , (b)  $\beta_0$  and  $\beta_2$ , and (c)  $\beta_1$  and  $\beta_2$  for clay, silt and sand. Figures also show the parameters from the previous studies by Brandenberg et al. (2010) and Wair et al. (2012).

Figure 2 also shows the regression parameters by Brandenberg et al. (2010) and Wair et al. (2012) for comparison. The results by Brandenberg et al. (2010) locate nearly the center of distributions obtained from the database, where the results by Wair et al. (2012) are slightly shifted from the center of distributions, but still within the range of the parameter distributions.

$$\beta_1 = 0.080 + \frac{0.0608}{\sigma_N} \tag{16}$$

$$\beta_2 = 0.0689 + 0.0381b_0 + \left(0.254 - \frac{0.0608}{\sigma_N}\right)b_1 \qquad (17)$$

#### 3 CALIBRATION OF SITE SPECIFIC VS PREDICTION MODEL WITH AVAILABLE N

This section describes the development of a site specific  $V_s$  prediction model where only N measurements are available from several borings, but no  $V_s$  measurements. The  $c_0$  and  $c_1$  in Equation (2) are estimated conditioned on the  $b_0$  and  $b_1$  measurements as follows:

$$\begin{bmatrix} c_0 \\ c_1 \end{bmatrix} = \begin{bmatrix} \hat{c}_0 \\ \hat{c}_1 \end{bmatrix} + \sum_{12} \sum_{22}^{-1} \begin{bmatrix} b_0 - \hat{b}_0 \\ b_1 - \hat{b}_1 \end{bmatrix}$$
 (11)

By substituting Equations (8), (9) and (10) into (11), the following expressions are obtained:

$$c_0 = 4.21 + 0.132b_0 - 0.132b_1 \tag{12}$$

$$c_1 = 0.0689 + 0.0381b_0 + 0.335b_1 \tag{13}$$

Similarly, the  $\sigma_{Vs}$  is obtained conditioned on  $\sigma_N$  as follows:

$$\sigma_{V_{S}} = 0.152 + 0.202\sigma_{N} \tag{14}$$

Therefore, substituting Equations (12), (13) and (14) into (4), (5) and (6),  $\beta_0$ ,  $\beta_1$  and  $\beta_2$  in Equation (3) are obtained conditioned on the  $b_0$ ,  $b_1$  and  $\sigma_N$  as follows:

$$\beta_0 = 4.21 + \left(0.0512 - \frac{0.0608}{\sigma_N}\right) b_0 - 0.132 b_1 \tag{15}$$

Urayasu, Japan where the lateral spread was observed after 2011 Tohoku earthquake (Ashford et al. 2011) is selected as an example site. Figure 3 shows the variation of  $N_{60}$  against  $\sigma'_{vo}$  for sand deposit beneath the fill. The figure shows that  $b_0$  and  $b_1$  in Equation (1) are 1.77 and 0.182, respectively. The standard deviation of  $\sigma_N$  is obtained as 0.663. Based on these variables,  $\beta_0$ ,  $\beta_1$  and  $\beta_2$  are obtained from Equations (15) to (17); hence the  $V_s$  prediction model conditioned on these measurements is obtained as follows:

$$\ln V_s = 4.11 + 0.172 \ln N + 0.166 \ln \sigma_{vo}' \tag{18}$$

Standard deviation is calculated based on Equations (14) as follows:

$$\sigma_{V_{S|N}} = 0.262 \tag{19}$$

By following this approach, the site specific  $V_s$  prediction models can be calibrated by using the global database and the available N measurements at application sites.

#### 4 CONCLUSIONS

The  $V_s$  prediction model conditioned on SPT N is discussed in this paper. This study focuses on the calibration of  $V_s$  prediction model with the site specific database, where previous studies mainly focuses on the improvement of the model based on soil type such as clay, silt and sand.

Simple regression parameters of  $\ln V_s$  and  $\ln N$  against  $\ln \sigma'_{vo}$  were computed from global database. Based on these analyses, means, standard errors and correlations of these regression parameters are obtained as a basis to develop the site specific  $V_s$  prediction models.

Methodology to obtain the site specific  $V_s$  prediction model is described when only N are available from several borings, but no  $V_s$  measurement. The proposed approach can reflect the trend observed in  $\ln N$  vs.  $\ln \sigma'_{vo}$  at application sites whereas previous studies have to assume the same site condition between where  $V_s$  prediction model was developed and the application site. This is a significant improvement to adjust the  $V_s$  prediction models to the local site conditions. The proposed approach can be applicable to any sites since no specific assumption exists behind the development of conditional  $V_s$  prediction model with N.

#### 5 REFERENCES

Grove, A.T. 1980. Geomorphic evolution of the Sahara and the Nile. In M.A.J. Williams & H. Faure (eds), *The Sahara and the Nile*: 21-35. Rotterdam: Balkema.

Jappelli, R. & Marconi, N. 1997. Recommendations and prejudices in the realm of foundation engineering in Italy: A historical review. In Carlo Viggiani (ed.), Geotechnical engineering for the preservation of monuments and his-

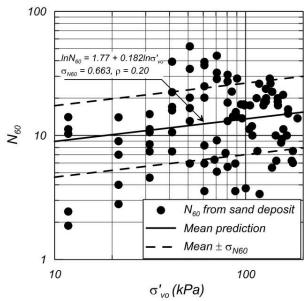


Figure 3. Variation of  $N_{60}$  for sand deposit beneath artificial fill against  $\sigma'_{\nu_0}$ .

torical sites; Proc. intern. symp., Napoli, 3-4 October 1996. Rotterdam: Balkema.

Johnson, H.L. 1965. Artistic development in autistic children. *Child Development* 65(1): 13-16.

Polhill, R.M. 1982. Crotalaria in Africa and Madagascar. Rotterdam: Balkema.

Wair, B. R., DeJong, J. T., and Shantz, T. 2012, Guidelines for Estimation of Shear Wave Velocity Profiles, PEER Report 2012/08, Pacific Earthquake Engineering Research Center, Headquarters at the University of California.

Brandenberg, S. J. and Bellana, N. and Shantz T. 2010, Shear wave velocity as function of standard penetration test resistance and vertical effective stress at California bridge sites, Soil Dynamics and Earthquake Engineering, 30, 1026-1035.

Arulnathan, R., et al. 2009. Vulnerability assessment of perimeter dike system at Oakland International Airport, TCLEE 2009 Conf.: 7th Int. Conf. on Lifeline Earthquake Eng., ASCE, Reston, VA.

Ashford, S. A., Boulanger, R. W., Donahue, J. L. and Stewart, J. P. 2011, Geotechnical Quick Report on the Kanto Plain Region during the March 11, 2011, Off Pacific Coast of Tohoku Earthquake, Japan, GEER Association Report No. GEER-025a (April 5, 2011)

Taiwan Strong Motion Instrument Program 2014, Engineering Geological Database for TSMIP, http://egdt.ncree.org.tw/ (last accessed, 03/21/2015).

National Research Institute for Earth Science and Disaster Prevention. 2014. Strong-motion Seismograph Networks (K-NET, KiK-net). <a href="http://www.kyoshin.bosai.go.jp">http://www.kyoshin.bosai.go.jp</a> (last accessed, April. 1, 2015).