

# INTERNATIONAL SOCIETY FOR SOIL MECHANICS AND GEOTECHNICAL ENGINEERING



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# Some thoughts about teaching Soil Mechanics to Civil Engineering undergraduates

**Manuel de Matos Fernandes**

**october 2016**

# Faculty of Engineering of University of Porto



Photo by Francisco Piqueiro

Since September 2000

# Position of UNIV. of PORTO in the field of CIVIL ENGINEERING in some rankings in 2016

- QS, Quacquarelli Symonds:      World    51-100  
   Europe    15-33
- NTU, National Taiwan Univ.:    World    58  
   Europe    13
- ARWU Shanghai Ranking:        World    78  
   Europe    28



# Teaching Soil Mechanics to Civil Eng. undergraduates

## Context of our work

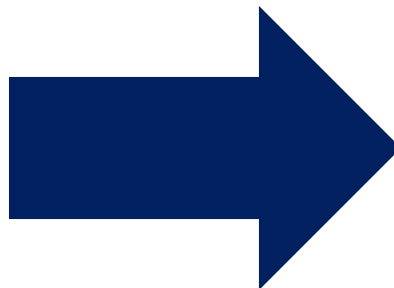
- Integrated master in Civil Engineering – 5 years course
- Soil Mechanics – 7<sup>th</sup> semester (in parallel with Concrete Structures, Roads, Project Management and Hydraulics)
- Introduction to Geotechnics – 8<sup>th</sup> semester
- Block of specialization disciplines in the 9<sup>th</sup> semester (Structures, Hydraulics, Geotechnics, Buildings, etc.)
- Dissertation in the 10<sup>th</sup> semester
- Around 160 students (this year)

# Teaching Soil Mechanics to Civil Eng. undergraduates

## Context of our work

- Semester with 13 weeks
- This allows 24/25 theoretical classes (1 hour)
- In complement, 12 practical classes (3 hours) to solve exercises and lab works

Physical indices  
Grain distribution  
Clay minerals  
Atterberg limits  
Classification



Shear strength and  
stress-strain  
relationships for  
sands and clays

# Students that have learned the **EFFECTIVE STRESS PRINCIPLE** past week





# City of Porto



Photo by José Paulo Andrade

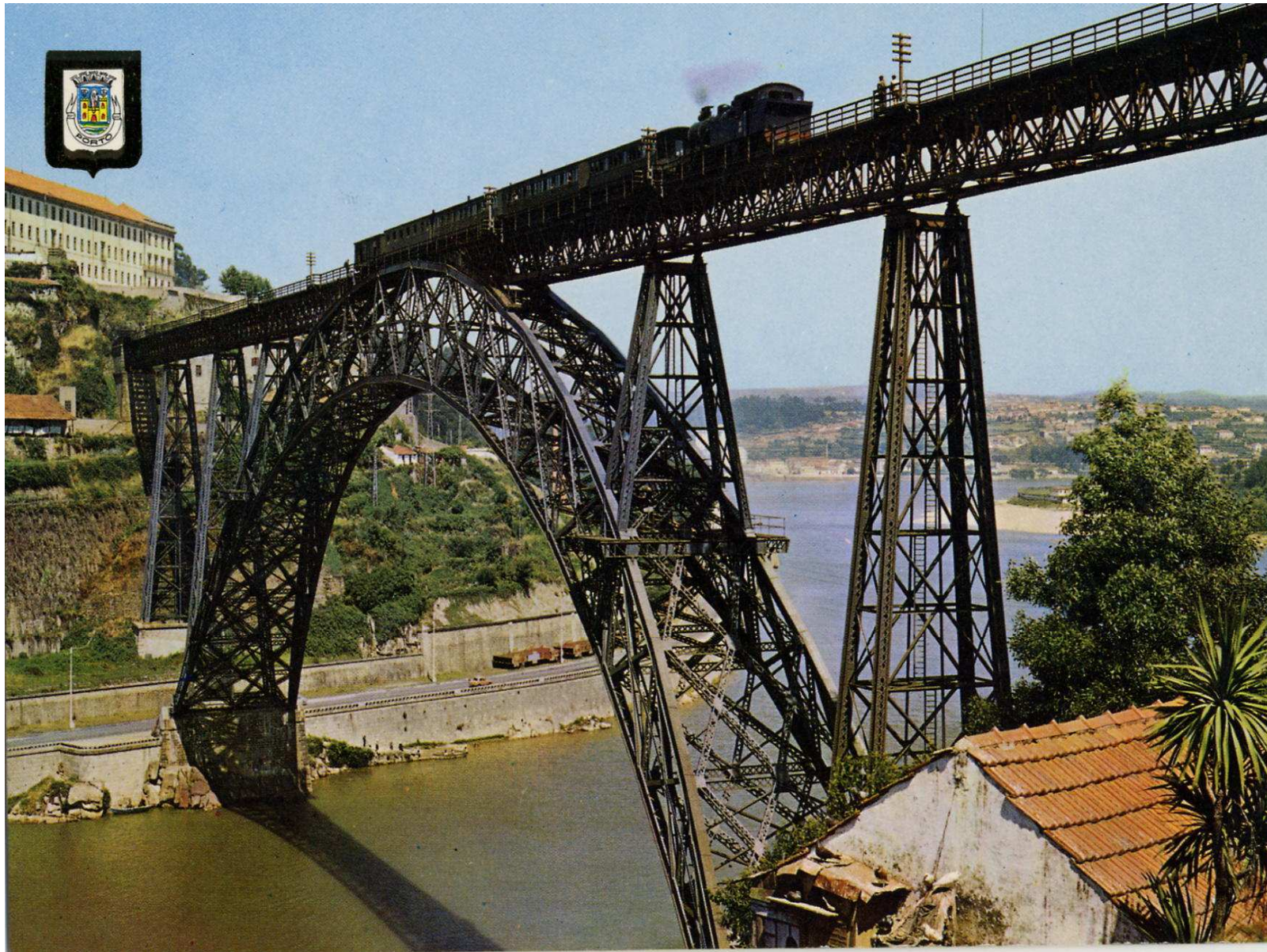


**A remarkable collection of  
bridges over river Douro  
estuary.**



**Photo by Francisco Piqueiro**





**Maria Pia Bridge, the largest iron arch in the world at the date of its conclusion, G. Eiffel and T. Seyrig, 1877**





**Luíz I Bridge, the unique XIX century iron bridge with two decks in the world, T. Seyrig, 1886**





**Arrábida Bridge, the largest reinforced concrete arch in the world at the date of its conclusion, Edgar Cardoso, 1963**



Photo by Luís Lousada Soares

**S. João Bridge, the prestressed concrete railway bridge of this type with the largest span (250 m) until today, Edgar Cardoso, 1991.**



**The best students dream to become bridge designers!**

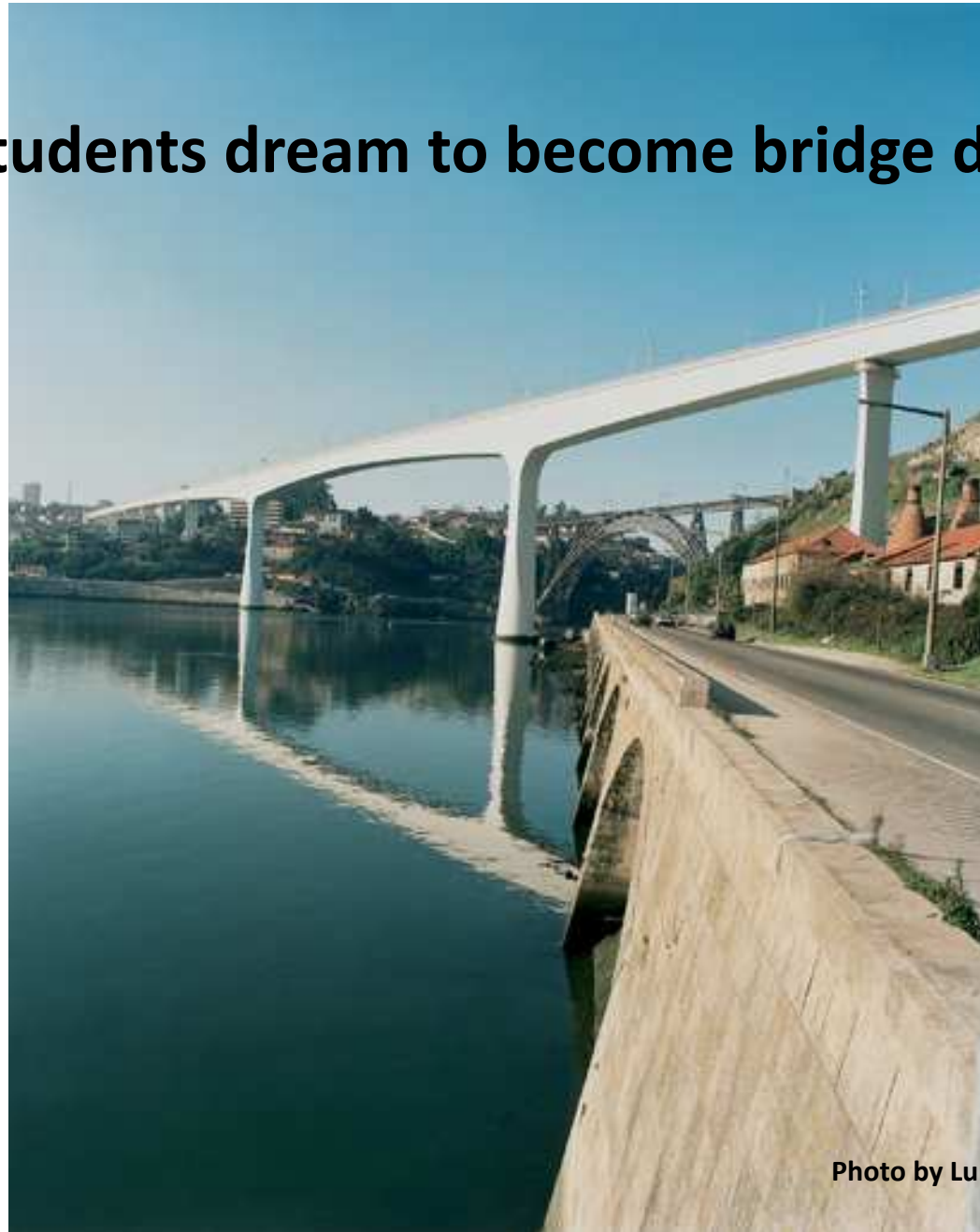


Photo by Luís Lousada Soares

- 3D heterogeneous mass
- Formed by grains, water and air
- Non elastic material. Failure
- Time dependent behaviour
- Influence of stress/geological history (overconsolidation, ageing, weathering)
- Dilatancy
- Effective stress and total stress analyses

# SOIL MECHANICS

- 3D heterogeneous mass
- Formed by grains, water and air
- Non elastic material. Failure
- Time dependent behaviour
- Influence of stress (geological) history (overconsolidation, ageing, weathering)
- Dilatancy
- Effective stress and total stress analyses

# SOIL MECHANICS

The natural science built by civil engineers.



# CONVENTIONAL CHAPTERS OF SOIL MECHANICS

Physical indices  
Grain distribution  
Clay minerals  
Atterberg limits  
Classification

Effective stress  
principle  
Permeability  
Seepage

Shear strength and  
stress-strain  
relationships for  
sands and clays

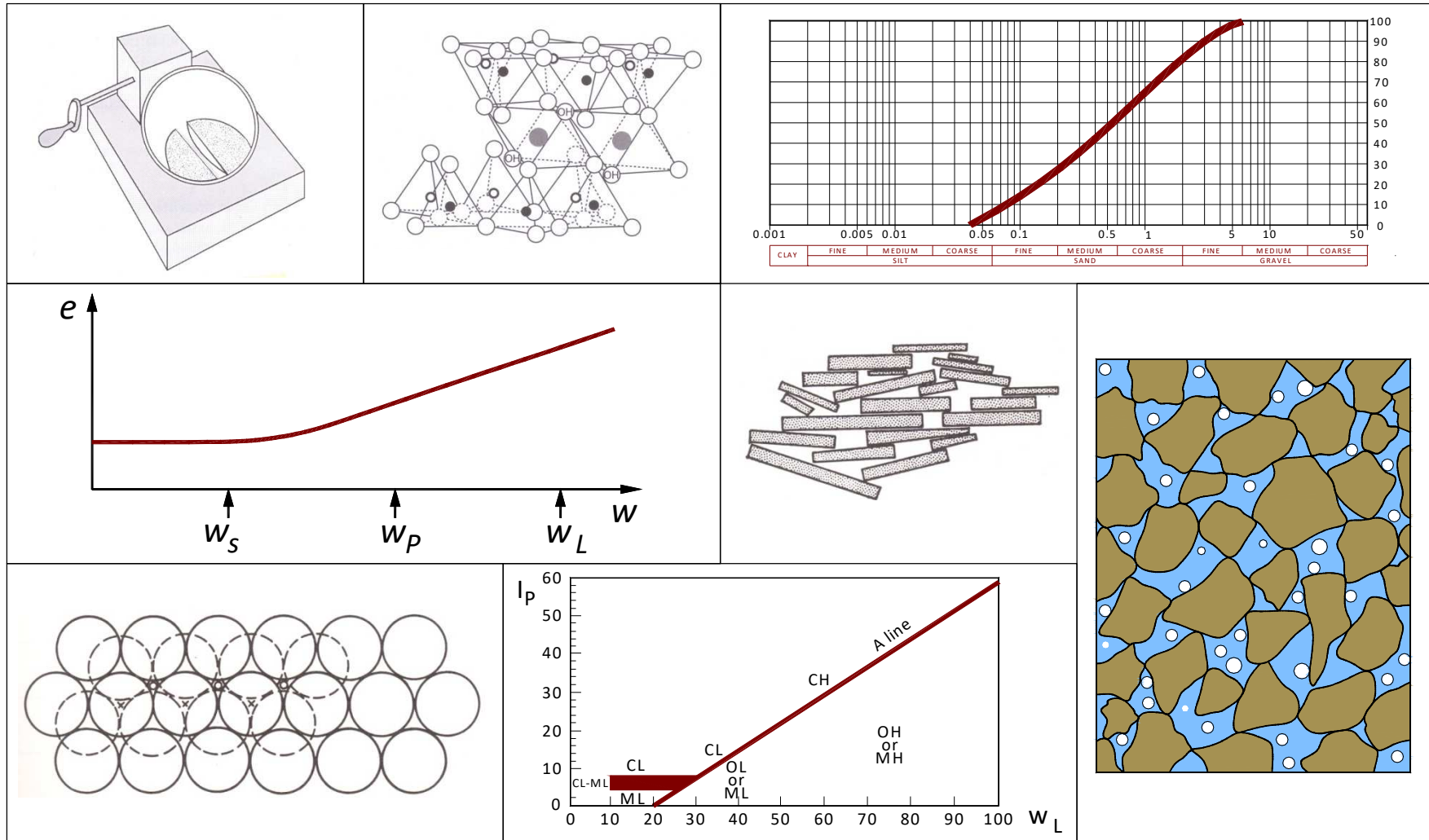
# Mechanics

Physical indices  
Grain distribution  
Clay minerals  
Atterberg limits  
Classification

Effective stress  
principle  
Permeability  
Seepage

Shear strength and  
stress-strain  
relationships for  
sands and clays

# Issues usually treated in the first chapter(s)



**GAP!**

Physical indices  
Grain distribution  
Clay minerals  
Atterberg limits  
Classification

Effective stress  
principle  
Permeability  
Seepage

Shear strength and  
stress-strain  
relationships for  
sands and clays



The contents of Soil Mechanics syllabus of the degree courses in many universities, as well as many text books, do not emphasize and analyse the strong relationships between the physical/identification parameters and the main trends of the mechanical behaviour of soils.

This is not in agreement with the capital importance they have in geotechnical practice.

In fact, most of the main decisions of an experienced engineer are made on the basis of the interpretation of the site geology and of the physical/identification parameters of the relevant soil layers.

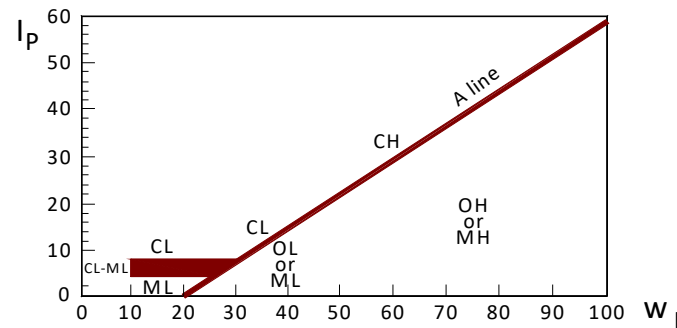
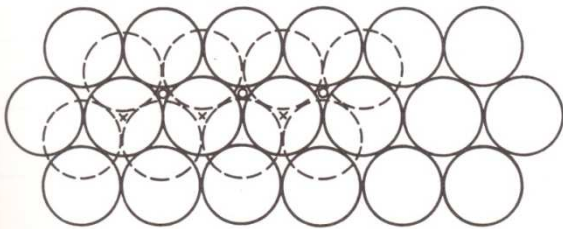
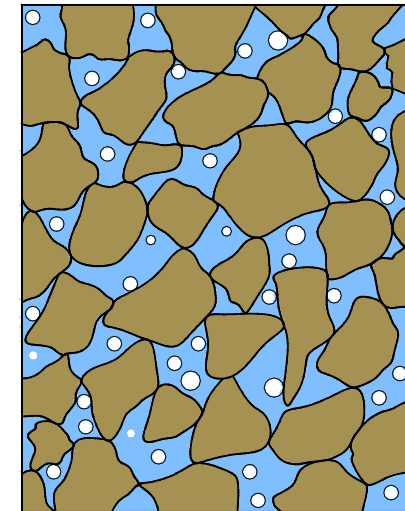
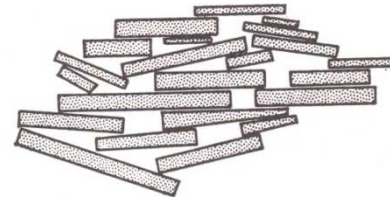
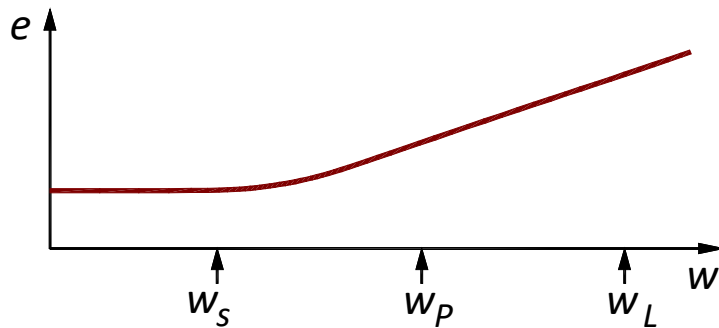
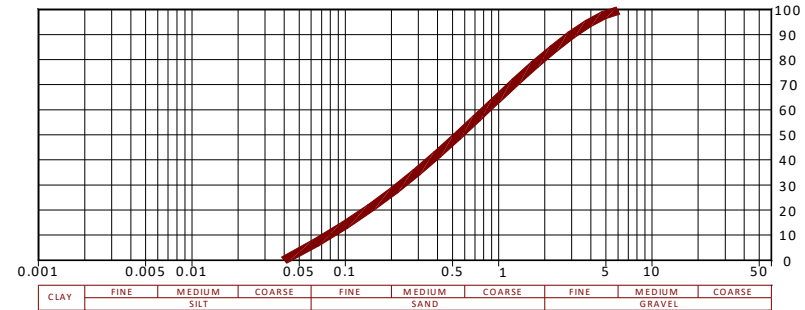
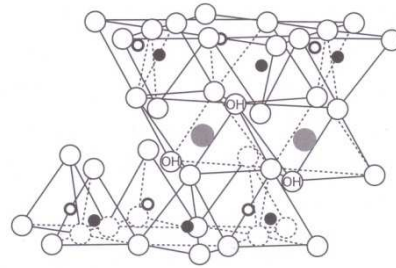
This means that experienced engineers have a clear idea on how the basic mechanical trends of soils are influenced by site geology and by the physical/identification parameters of the relevant soil layers.

Why this matter is not discussed in detail in our Soil Mechanics courses and books?

Is it impossible to obtain this skill at the University?

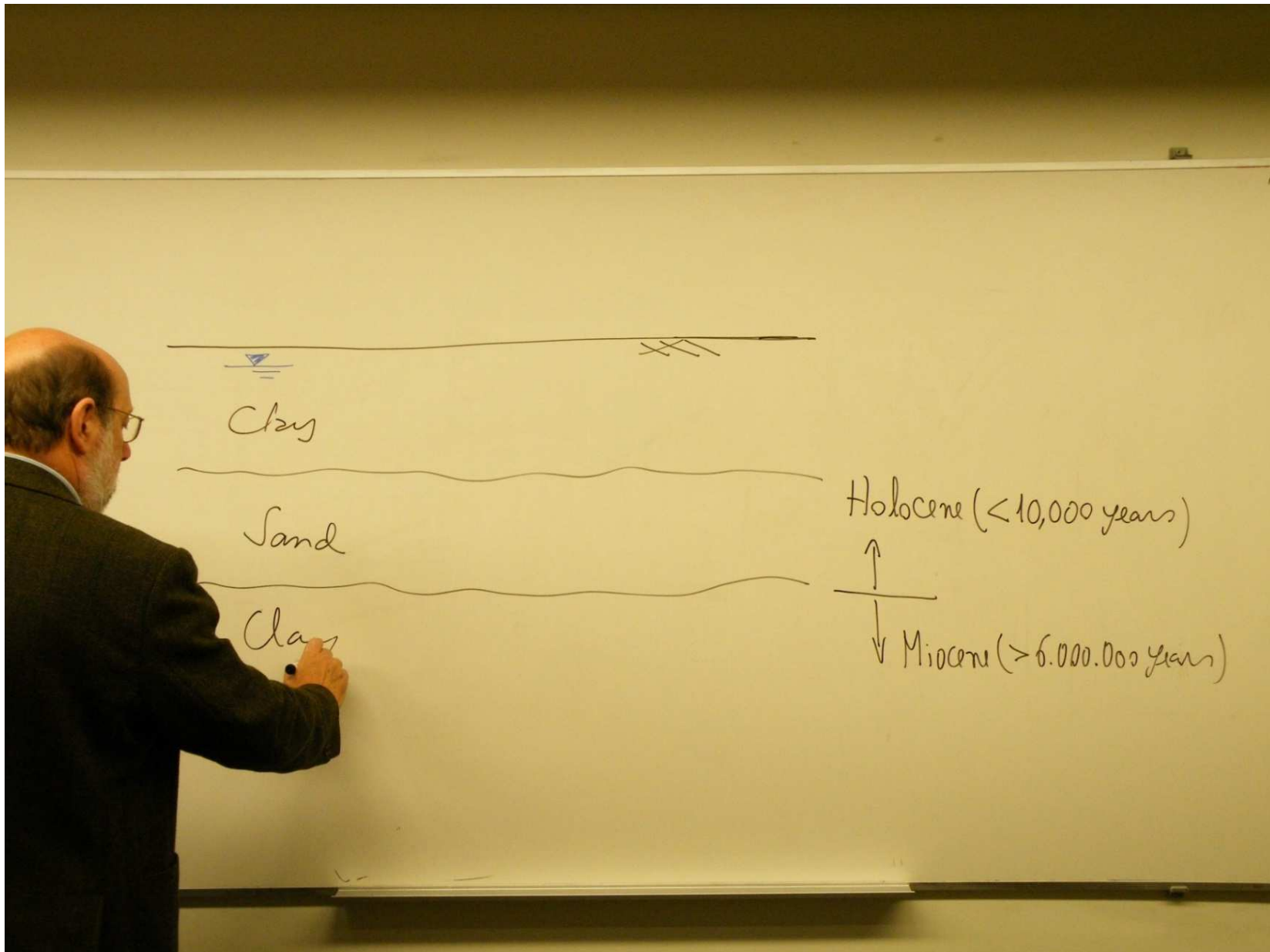
# We reflect on the soil at micro-scale: mineral particle or sample

Physical indices  
Grain distribution  
Clay minerals  
Atterberg limits  
Classification

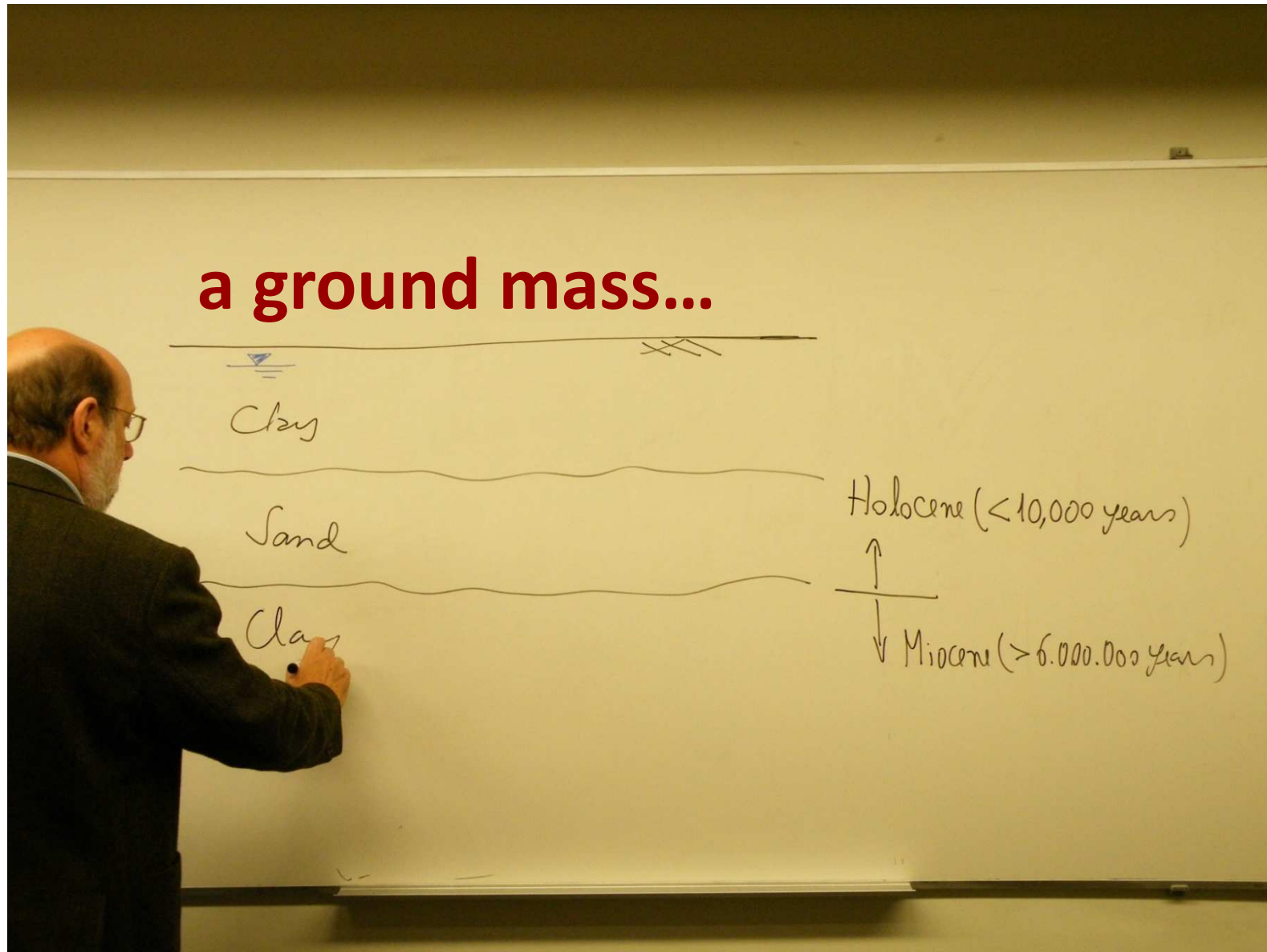




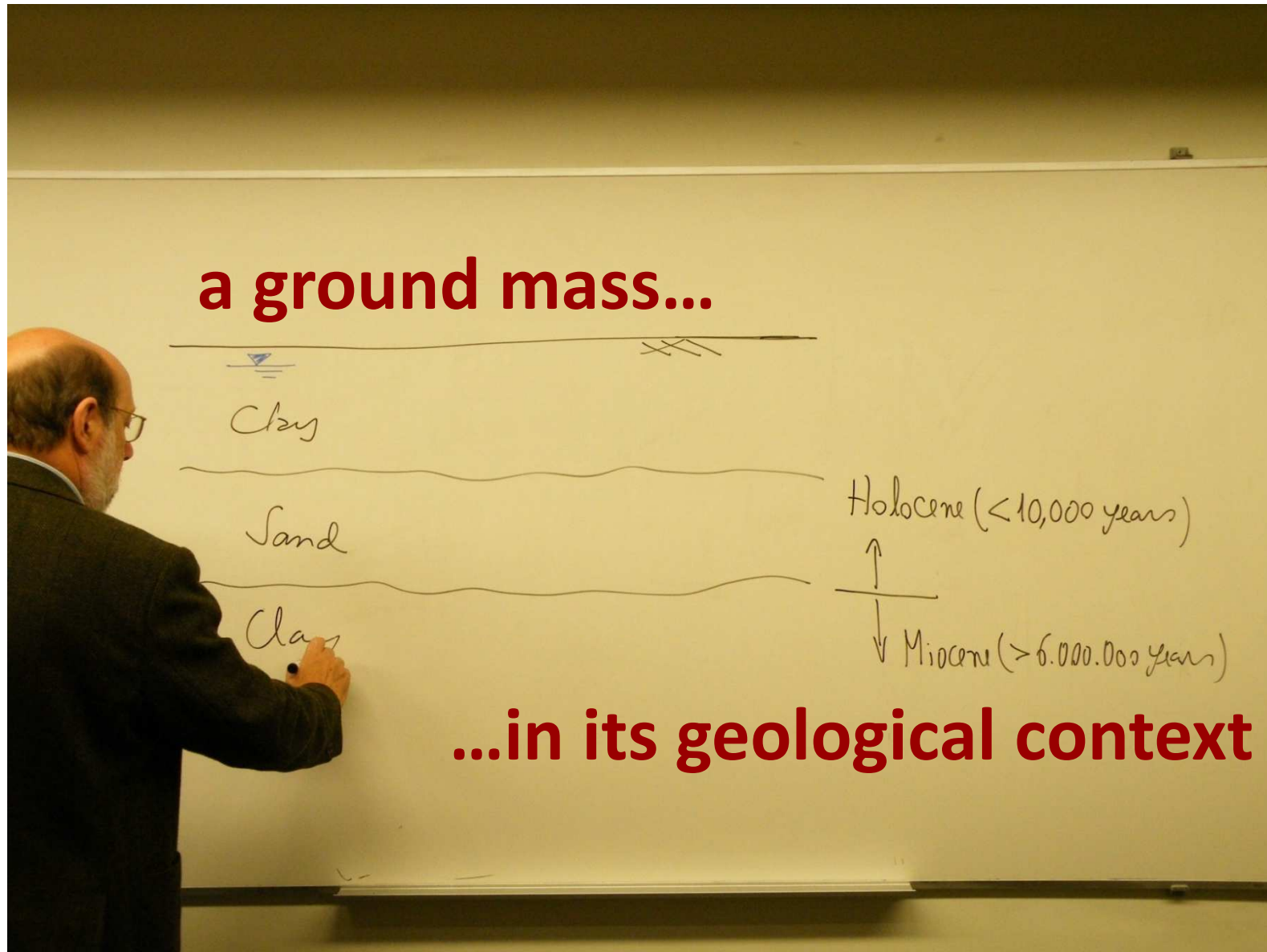
# But we should in the following think macro!



**But we should in the following think macro!**



**But we should in the following think macro!**



Physical indices  
Grain distribution  
Clay minerals  
Atterberg limits  
Classification

Basic trends of  
sedimentary sands and  
clays and of residual soils

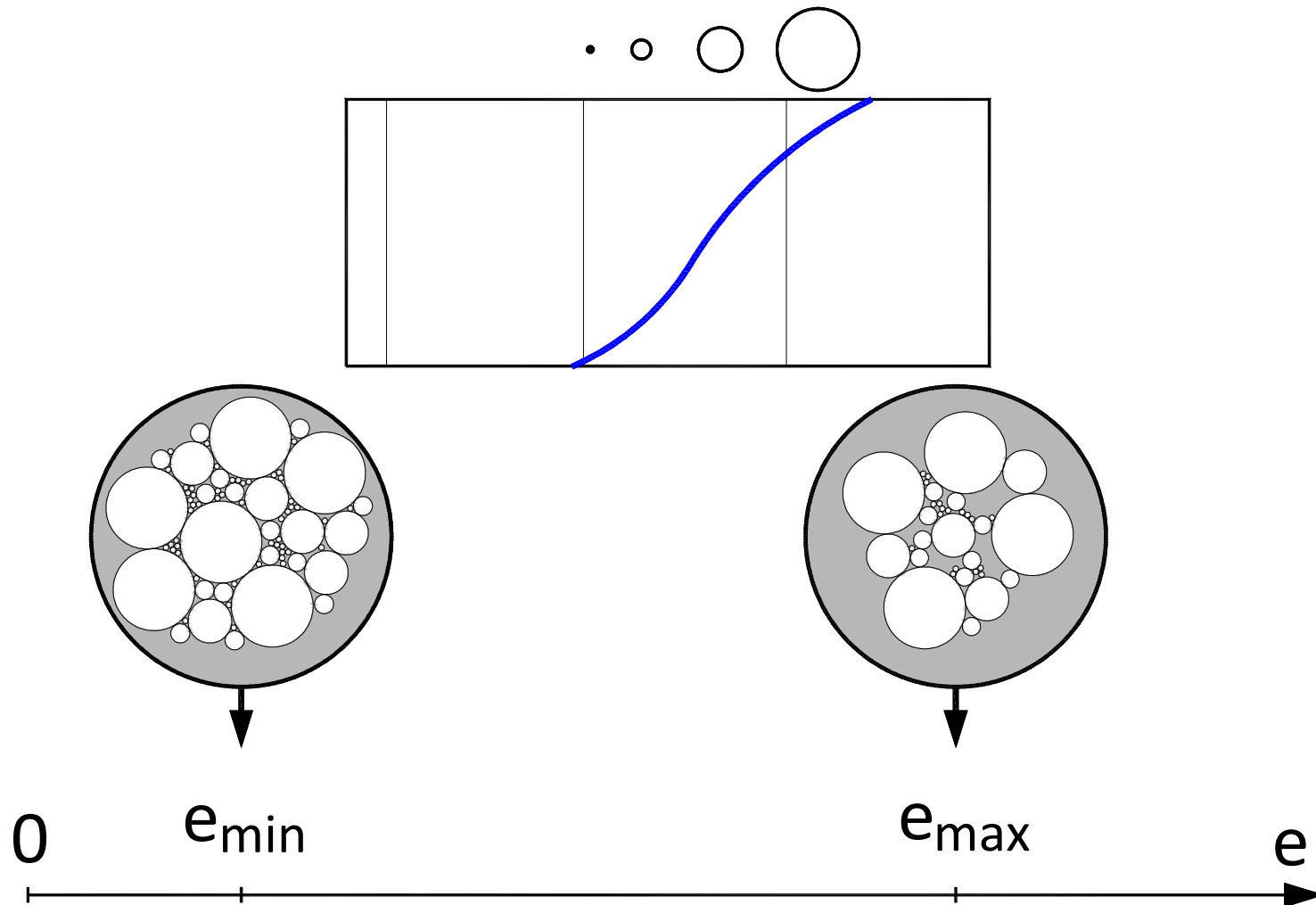
Effective stress  
principle  
Permeability  
Seepage

**This is a good time  
to discuss these matters!**

Shear strength and  
stress-strain  
relationships for  
sands and clays



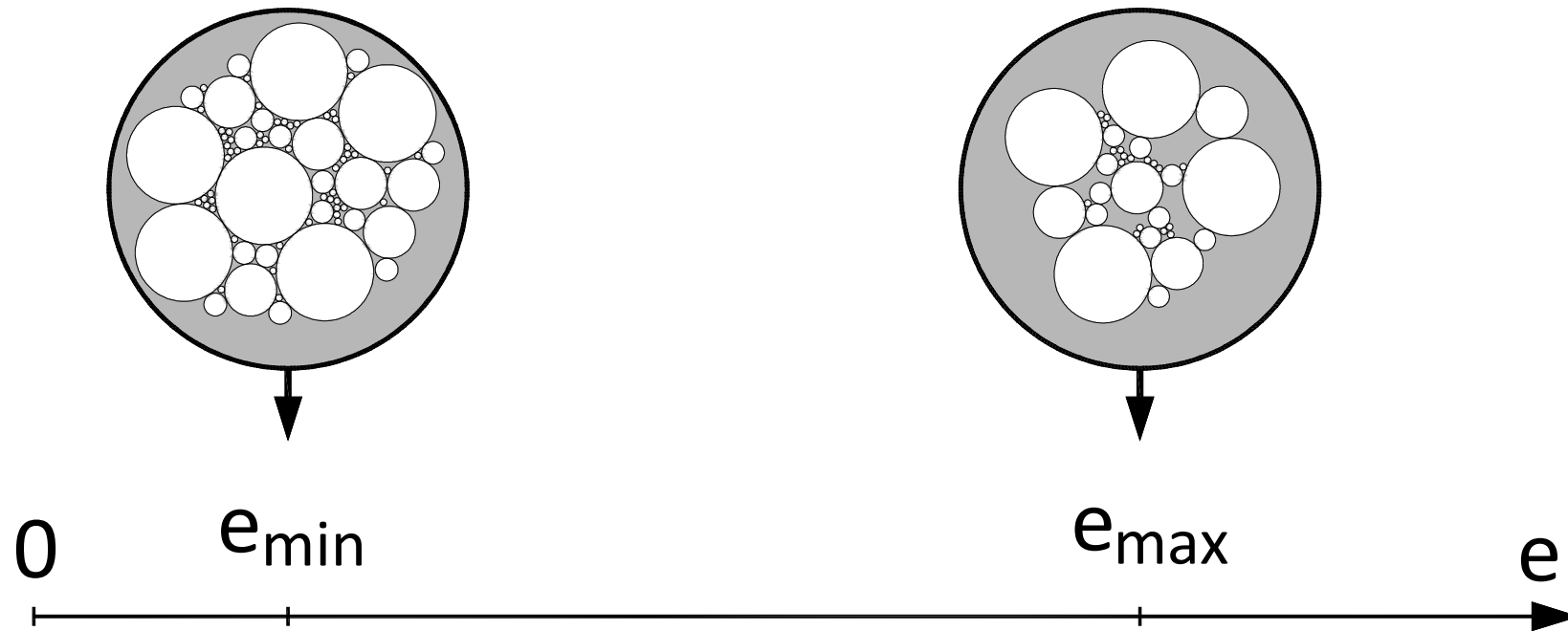
## $e_{\min} - e_{\max}$ interval for sands



## SIMPLE, ESSENTIAL, BUT OFTEN OMITTED QUESTIONS!

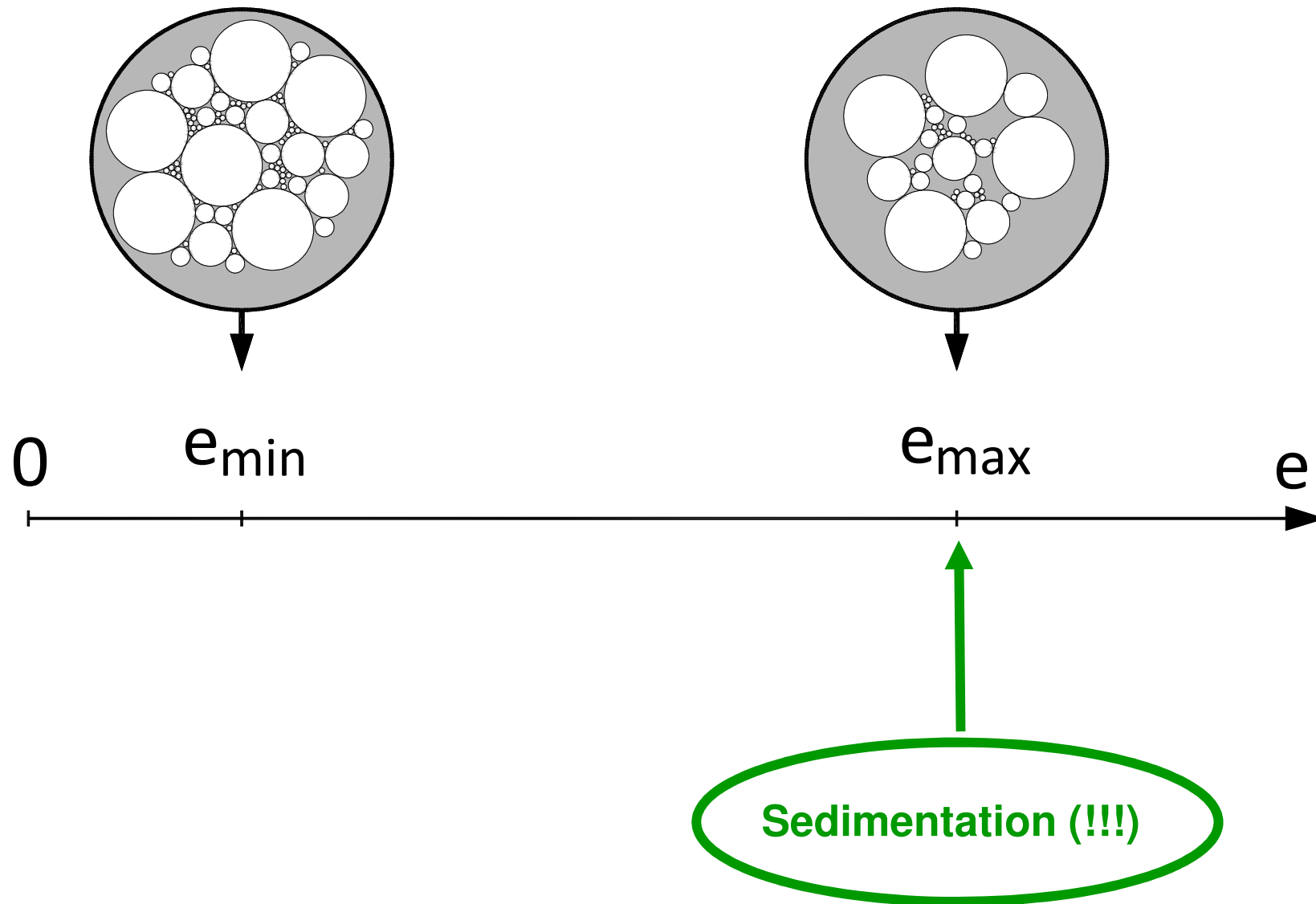
- **Where is the sand just after the sedimentation?**
- Which natural mechanisms lead to a progressive reduction of the void ratio?
- What are the consequences of such reduction to the response of the soil to static and dynamic loading?
- How can we prevent a poor performance if the natural void ratio is close to  $e_{max}$ ?
- If at a given site we have two sandy layers, how can we compare their density index?

Where is the sand just after the sedimentation?!

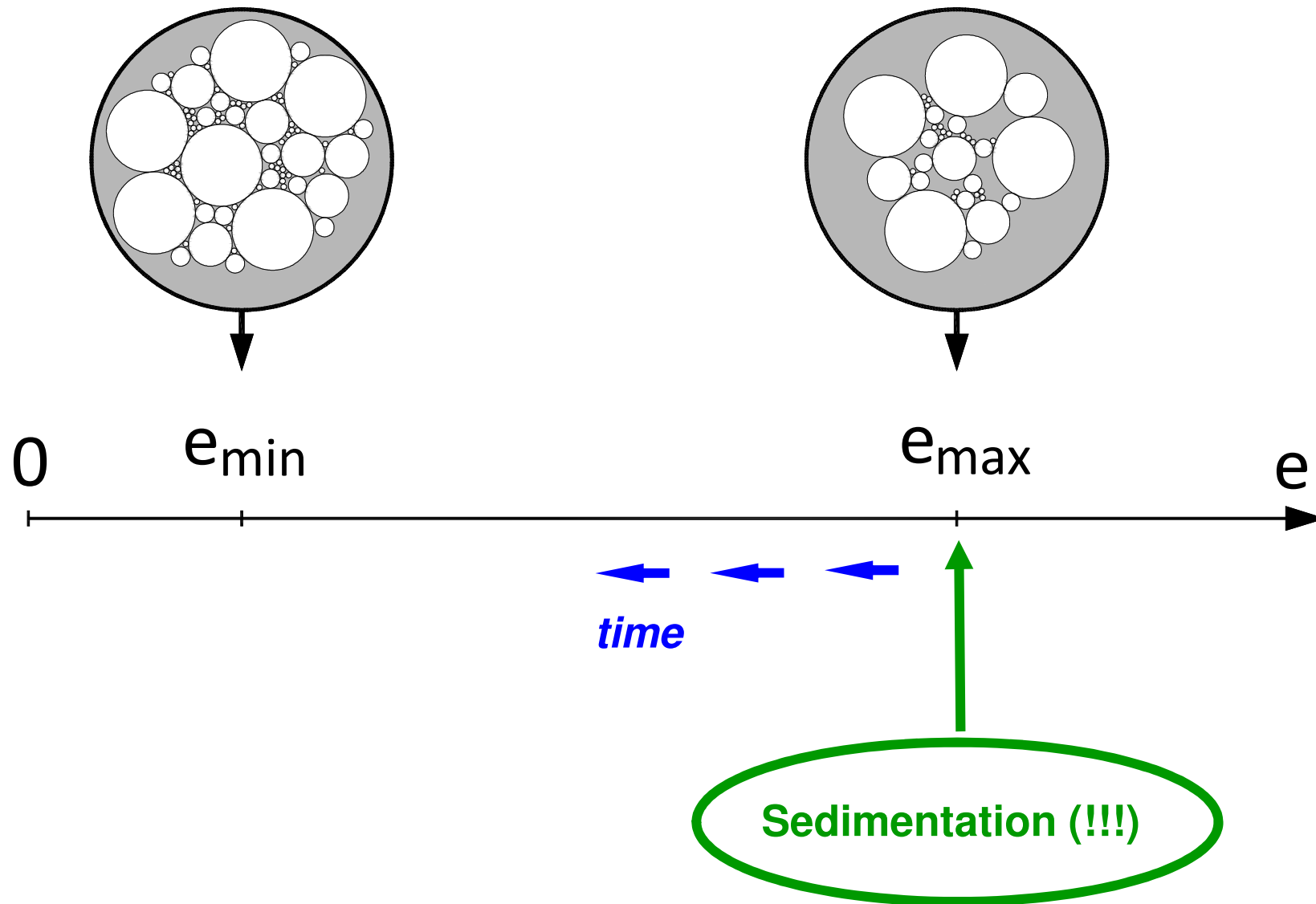




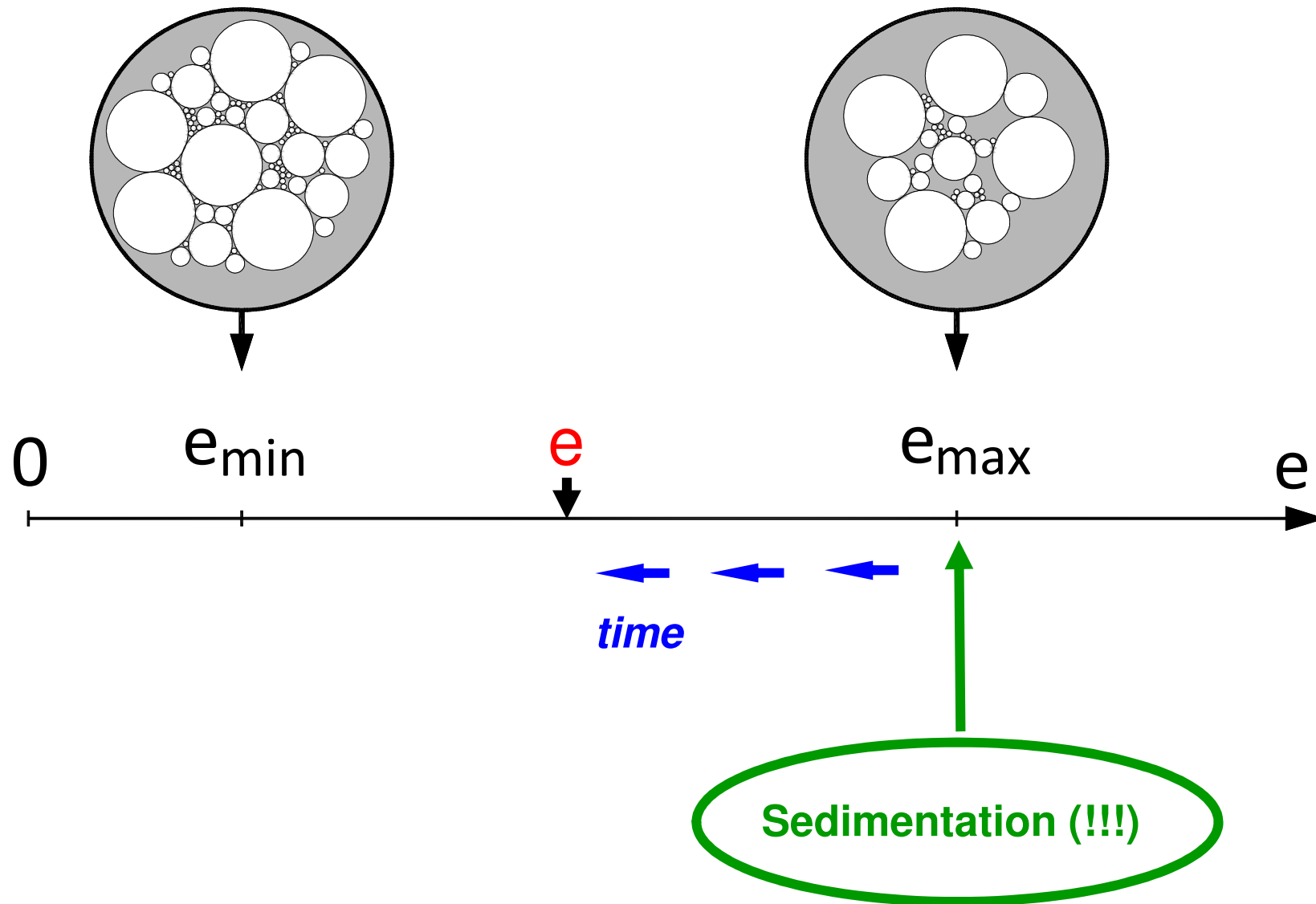
Where is the sand just after the sedimentation?



# Where is the sand just after the sedimentation?

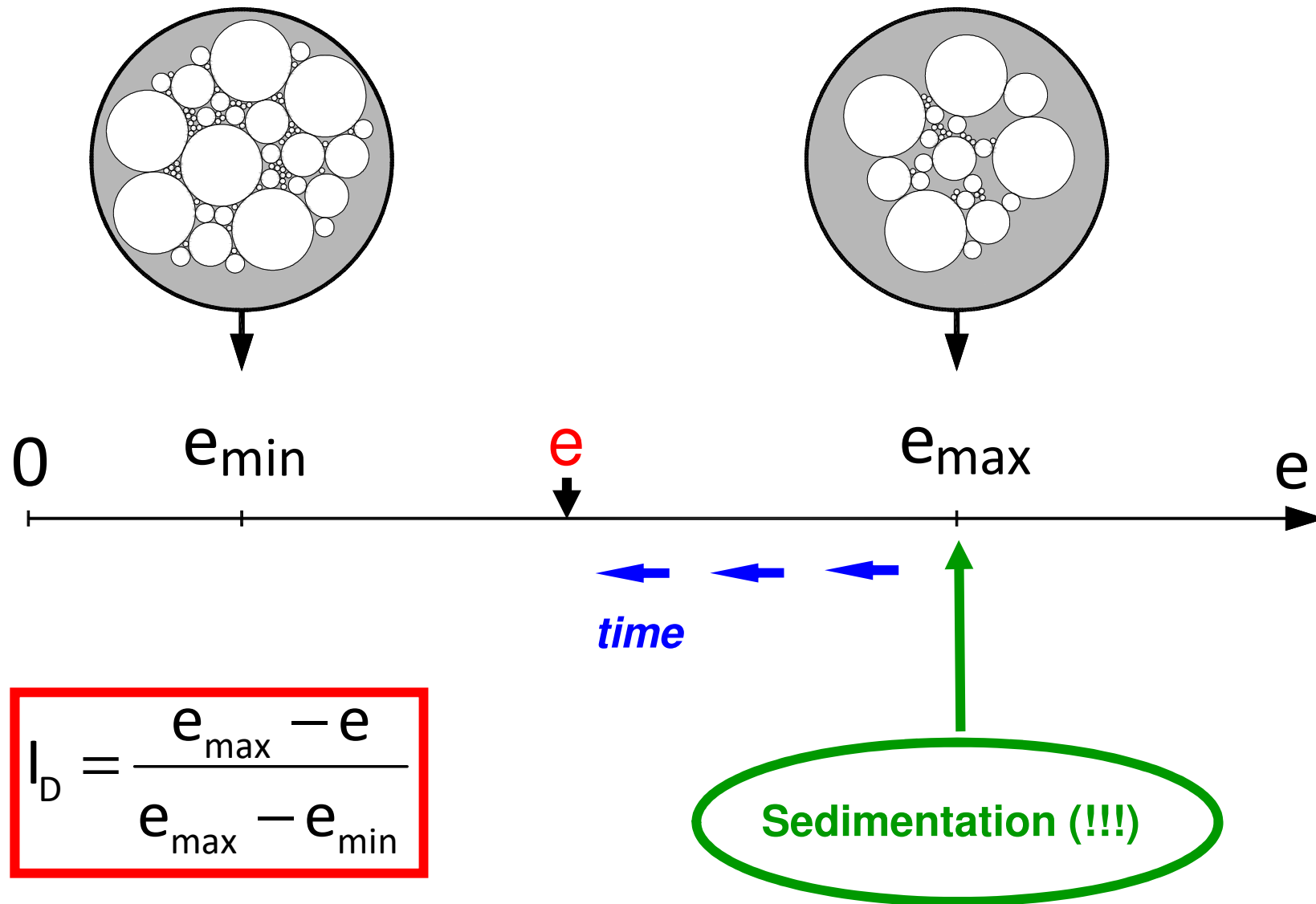


# Where is the sand just after sedimentation?





# Where is the sand just after sedimentation?



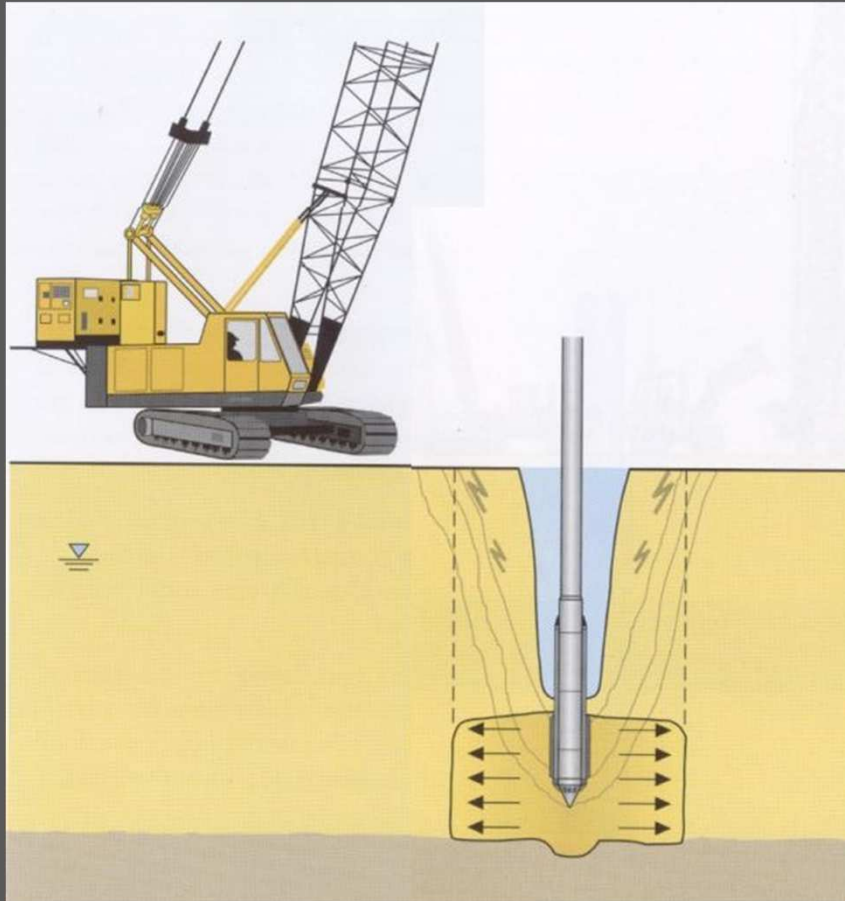
# How does Nature improve loose sands?



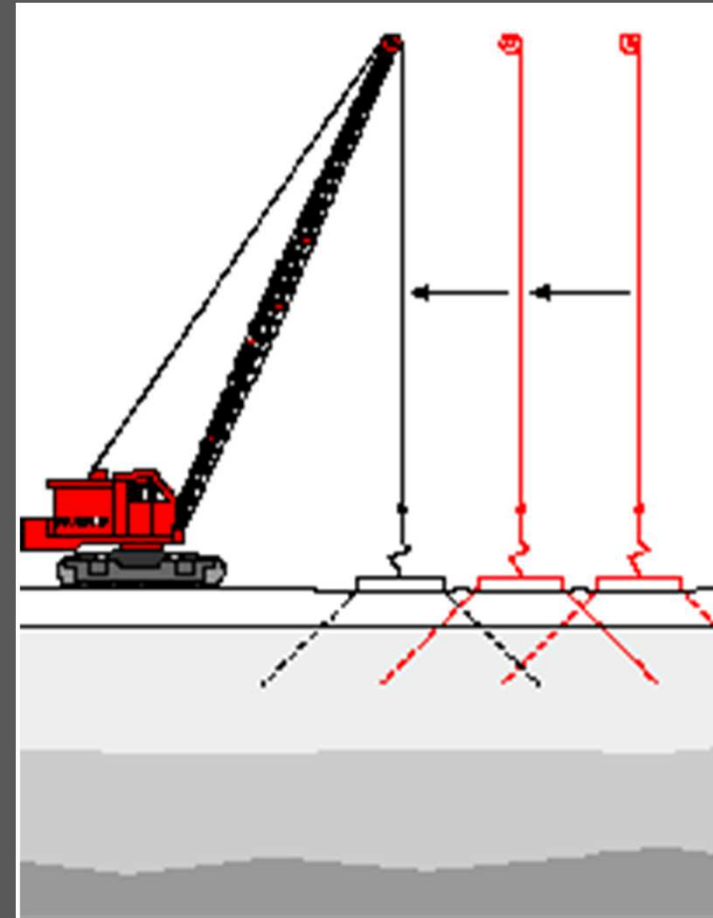
Kobe, Japan, 1995 earthquake

Photo by António Gomes Coelho

How can we prevent a poor performance if the natural void ratio is close to  $e_{max}$ ?



Vibrocompaction



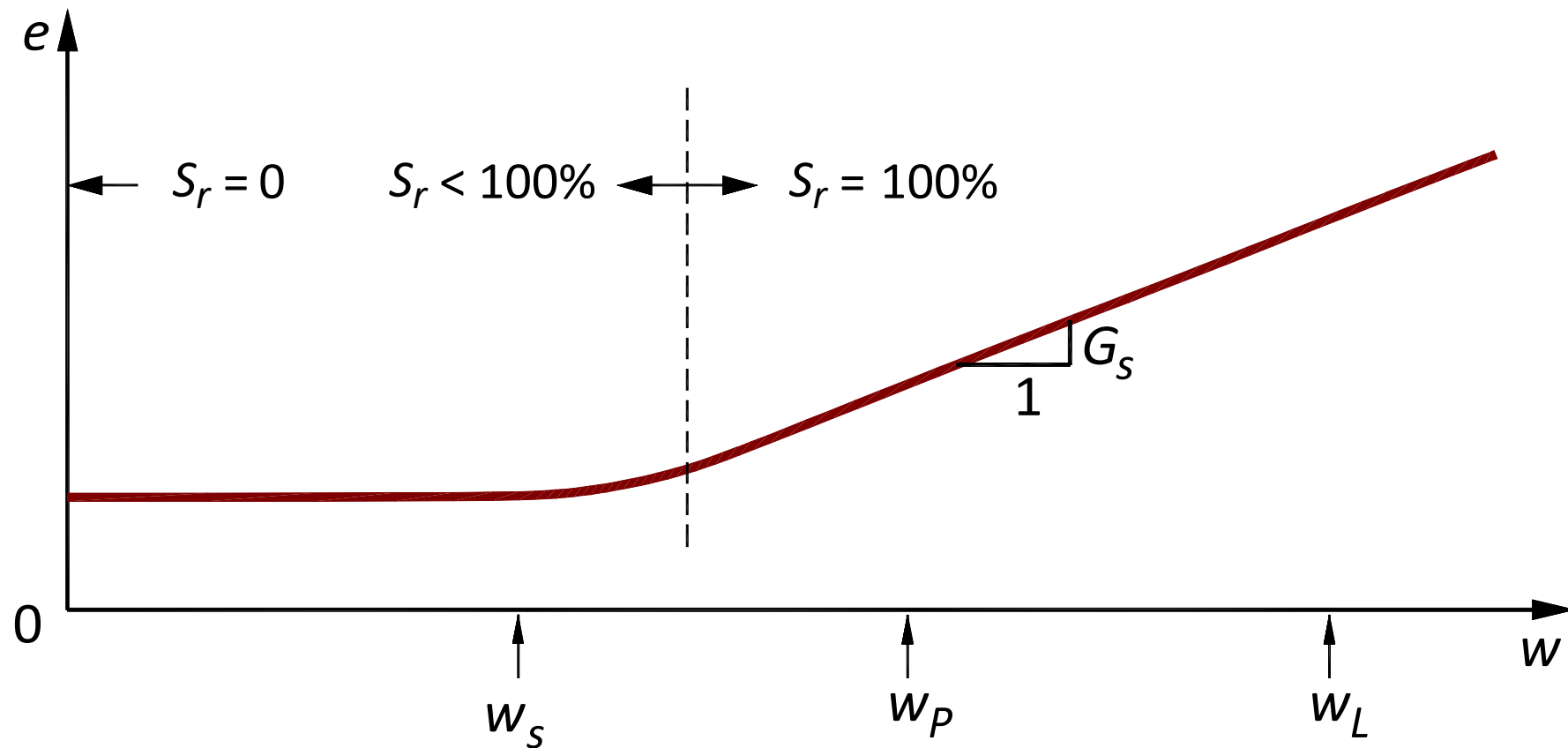
Dynamic compaction

## SIMPLE, ESSENTIAL, BUT OFTEN OMITTED QUESTIONS!

- **Where is the sand just after the sedimentation?**
- Which natural mechanisms lead to a progressive reduction of the void ratio?
- What are the consequences of such reduction to the response of the soil to static and dynamic loading?
- How can we prevent a poor performance if the natural void ratio is close to  $e_{max}$ ?
- **If at a given site we have two sandy layers how can we compare their density index?**



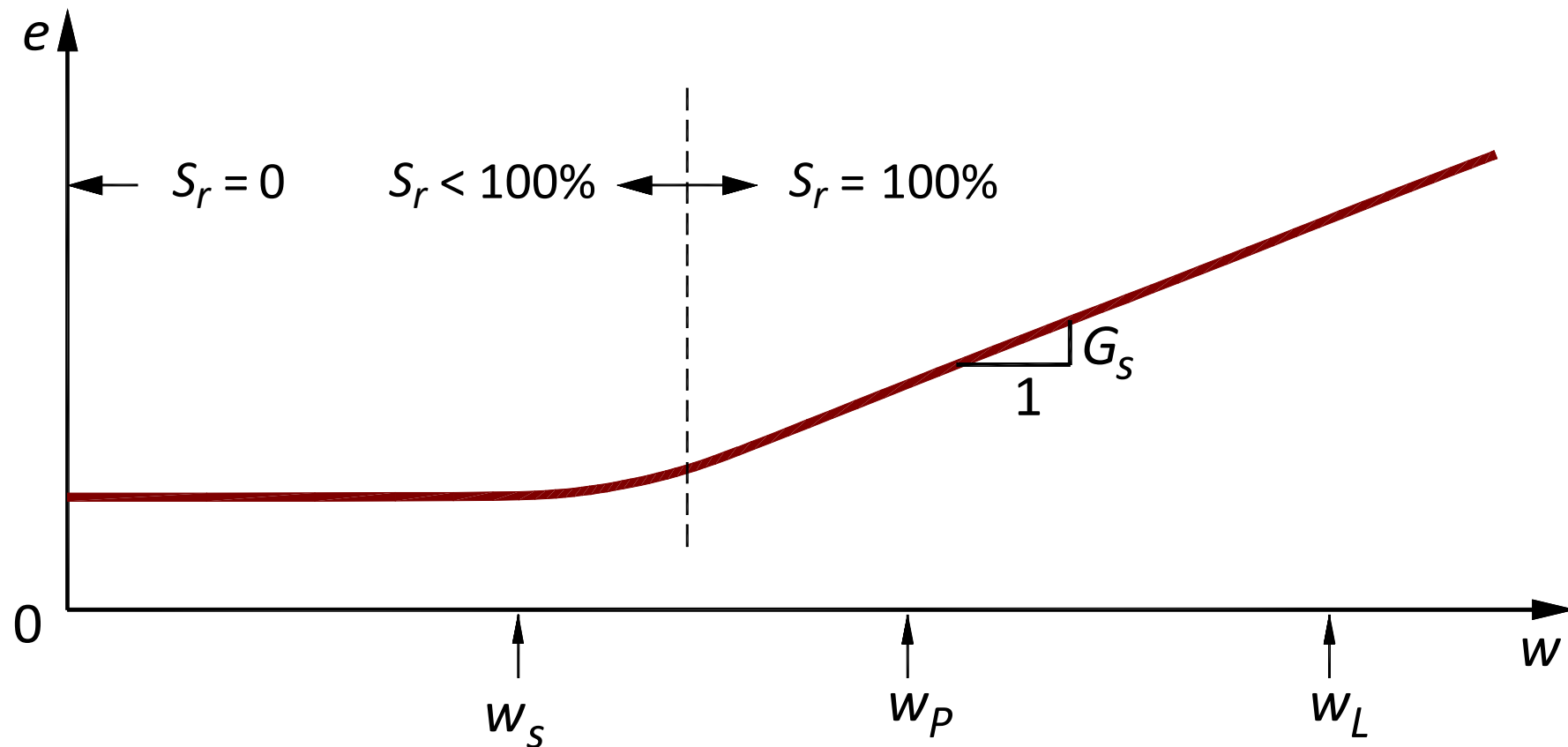
# Atterberg limits for clayey soils



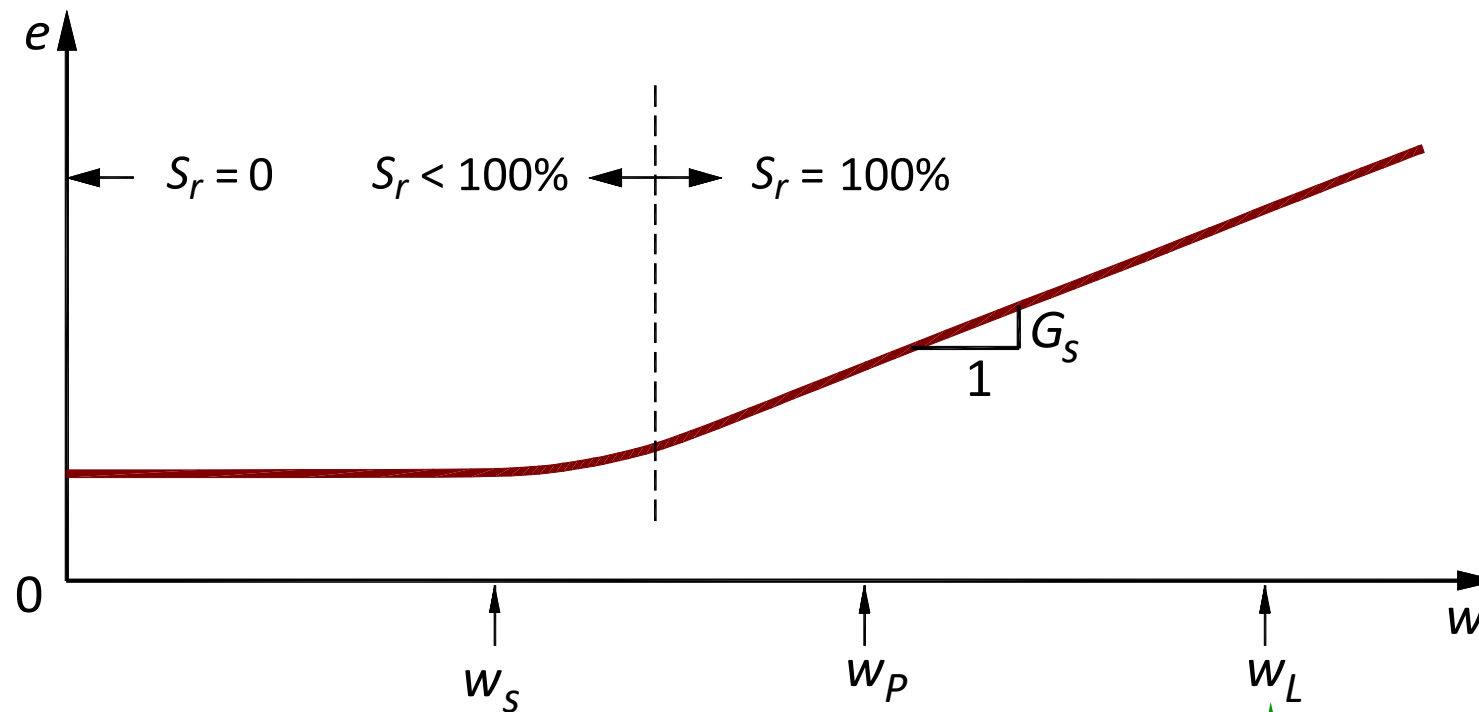
## SIMPLE, ESSENTIAL, BUT OFTEN OMITTED QUESTIONS!

- Where is the clay just after the sedimentation?
- How does Nature improve clayey soils?
- What are the consequences of such reduction to the response to static loading?
- If we apply a static load on a clay whose water content is close to  $w_L$ , what can we expect?
- How can we prevent such poor performance?
- If at a given site we have two clayey layers, how can we compare their consistency index?

# Where is the clay just after the sedimentation?!



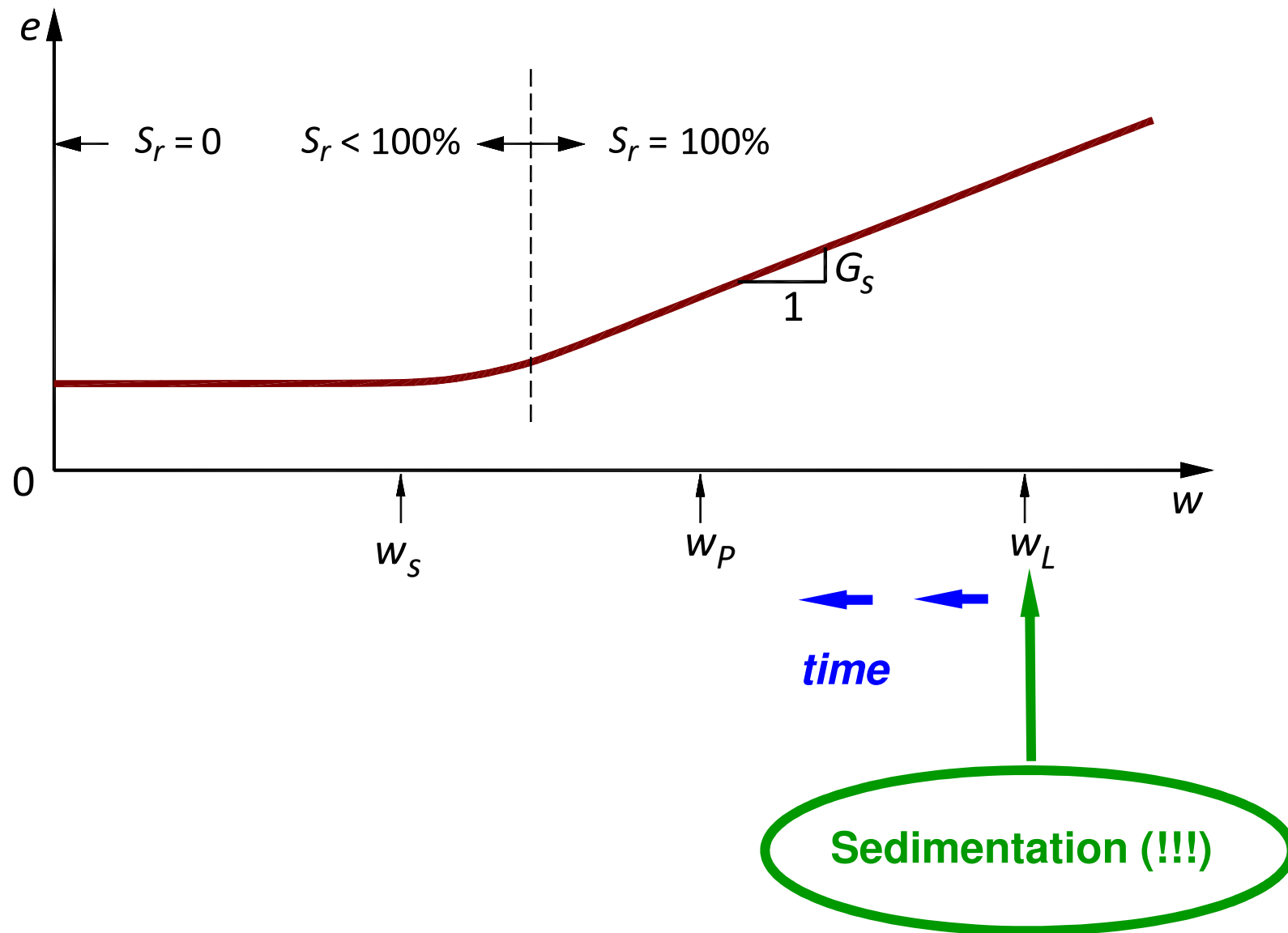
# Where is the clay just after the sedimentation?



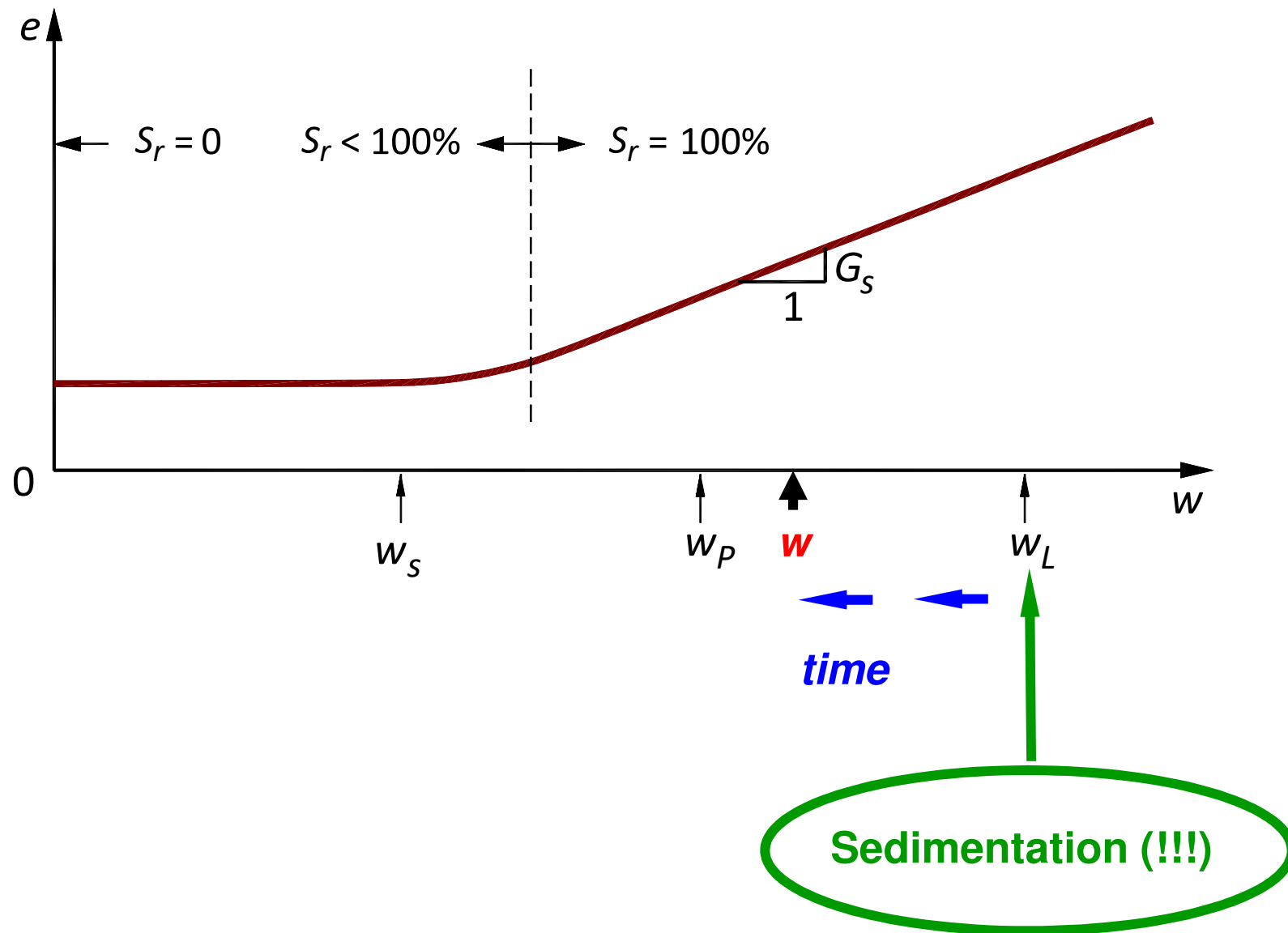
**Sedimentation (!!!)**



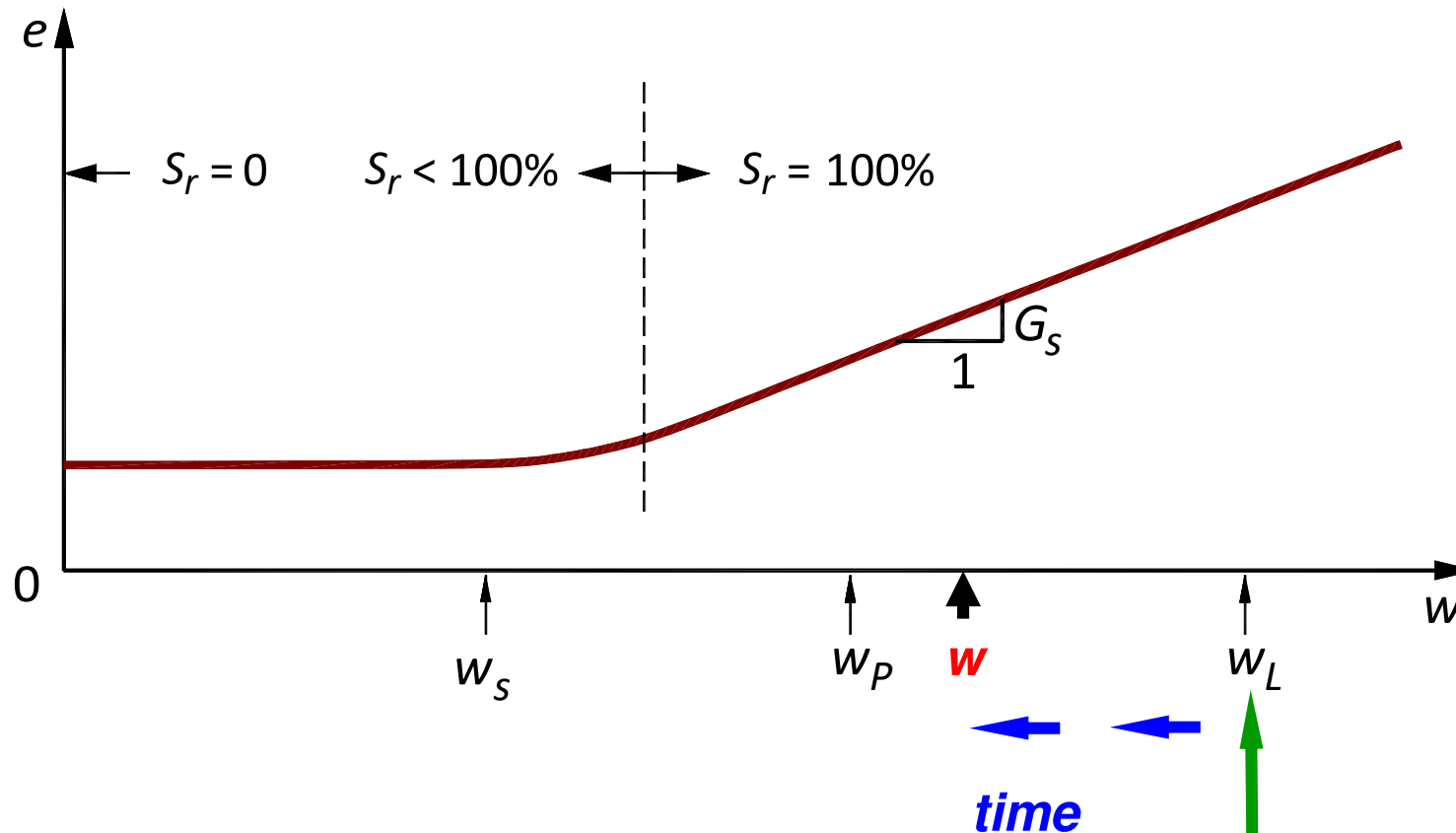
# Where is the clay just after the sedimentation?



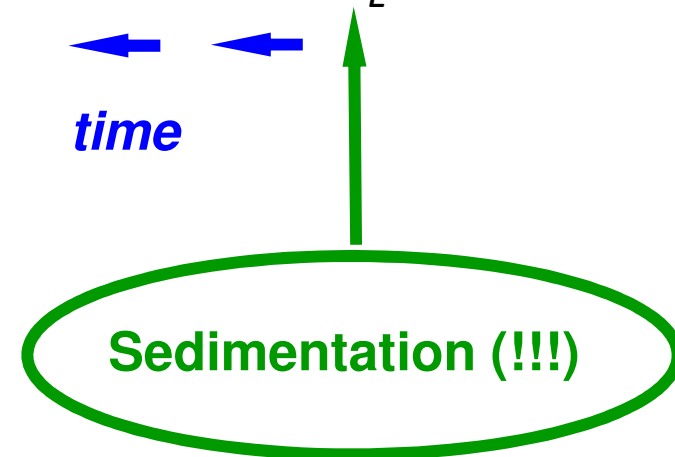
# Where is the clay just after the sedimentation?



# Where is the clay just after the sedimentation?

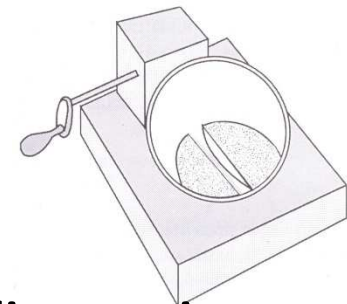


$$I_C = \frac{w_L - w}{w_L - w_p}$$



## Some topics for discussion:

- this idea is a simplification, and should be taken as a basic approximation (as will be observed in the next slide);
- further, there are exceptions to this idea; we will have opportunity to comment these exceptions (quick clays, etc.);
- if the lab test for  $e_{max}$  is basically a simulation of a grain pack of a sand that has just sedimented, why the liquid limit is determined through this strange test?!

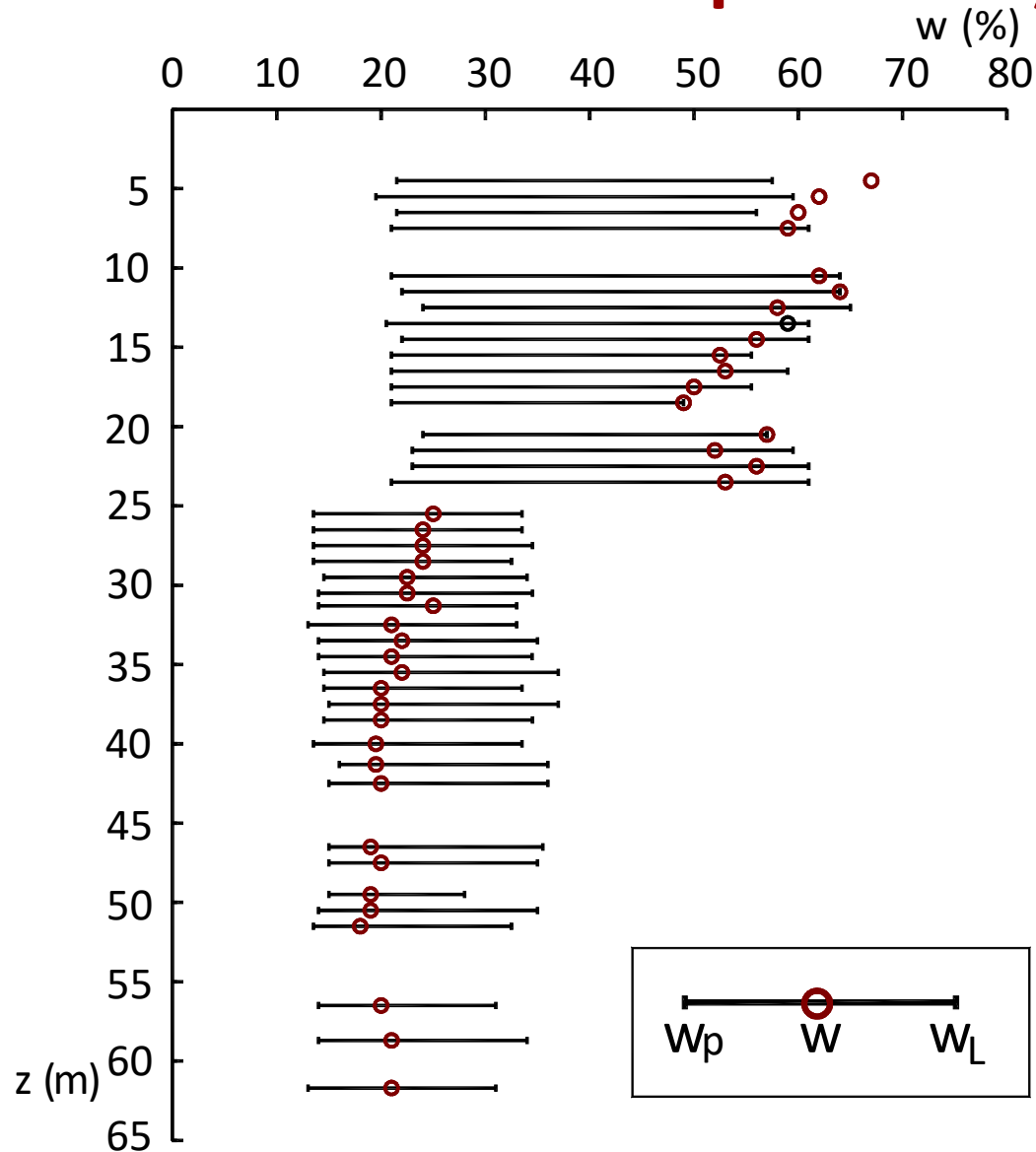


- Since it would not be feasible to replicate in the lab the sedimentation process for fine soils, the tests for determining  $w_L$  were conceived in order to provide a result of the water content corresponding to a very small consistency of the soil.



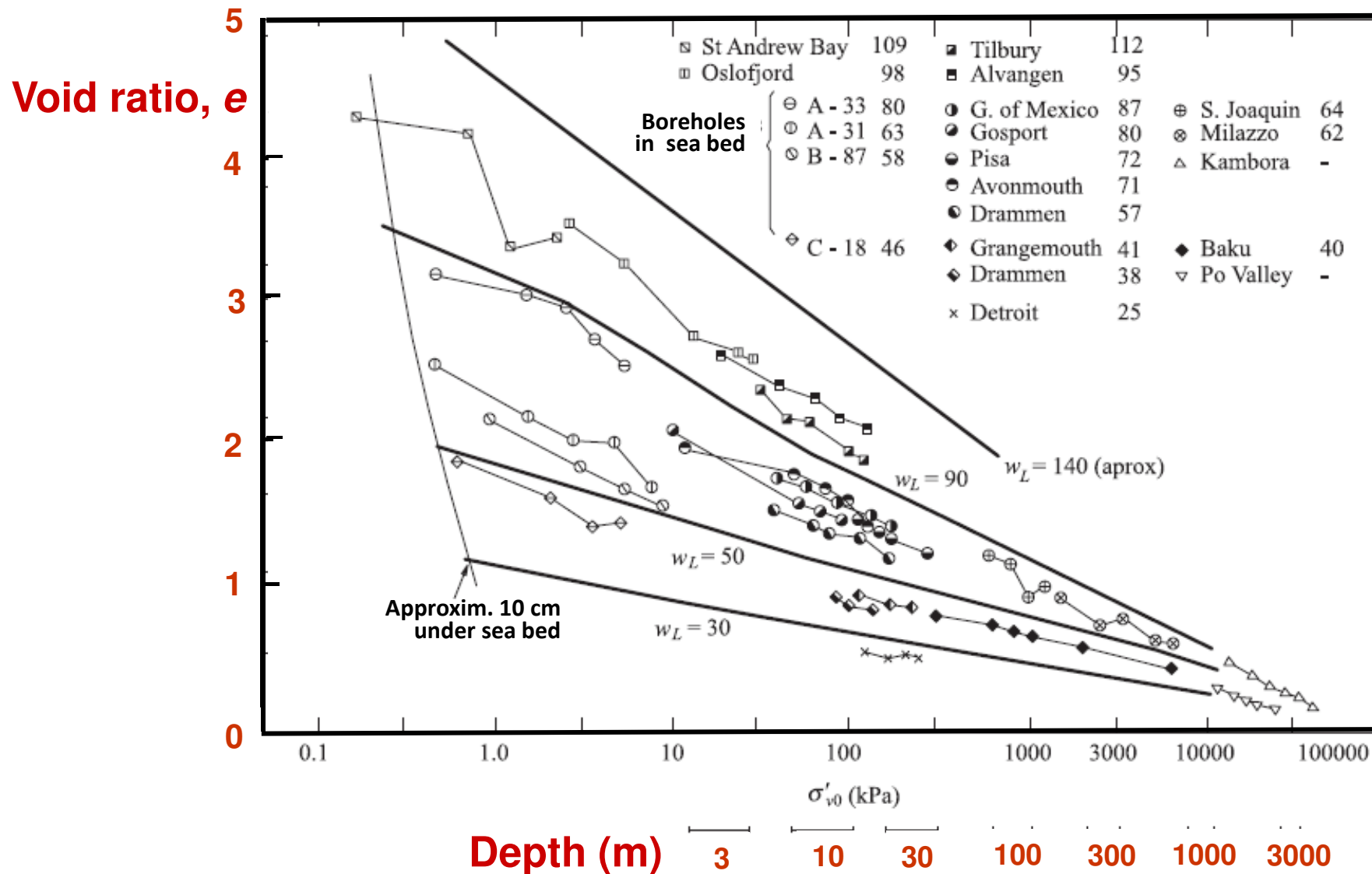
# Where is the clay just after the sedimentation?

## How does Nature improve clayey soils?



Burland, 1990

# How does Nature improve clayey soils?



A. W. Skempton, "The consolidation of clays by gravitational compaction", 1970

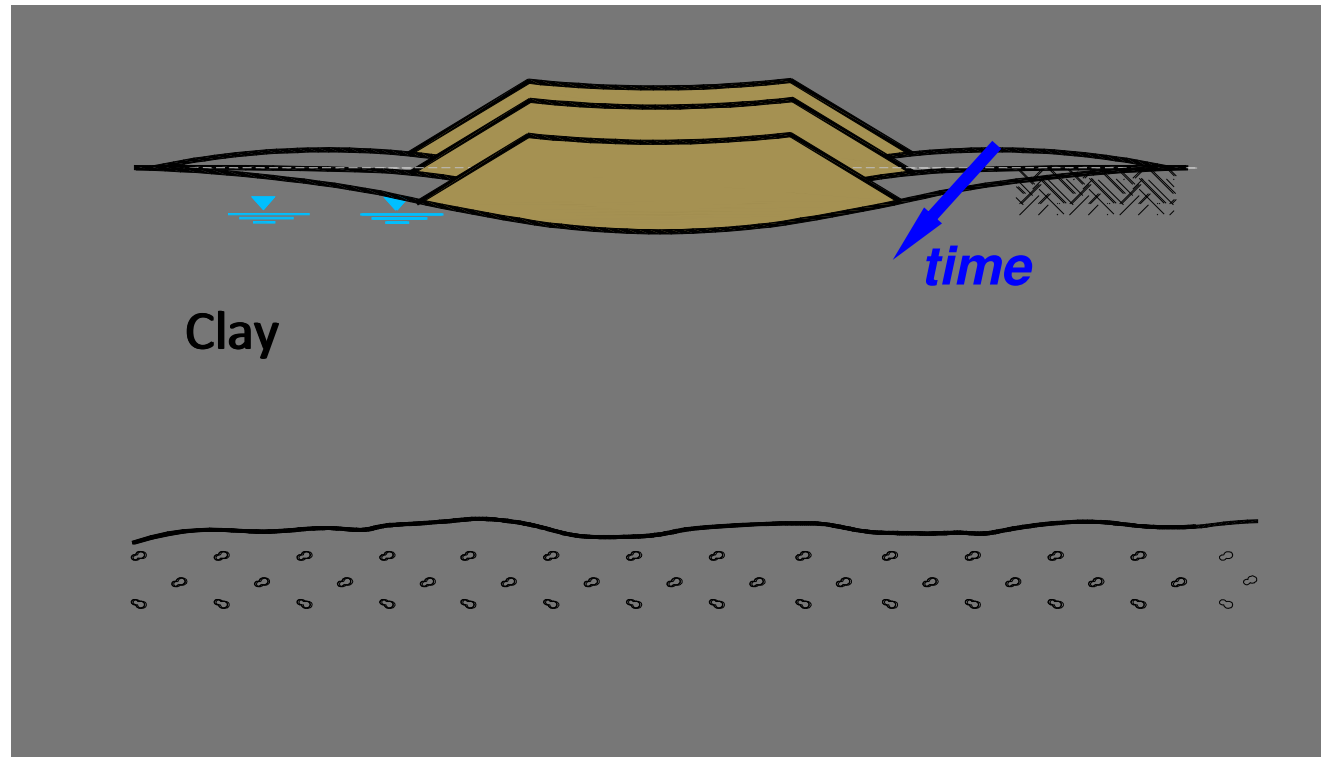
If a static load is applied on a clay whose water content is close to  $w_L$ , what can be expected?



Basilica de Guadalupe and Templo de Las Capuchinas, Mexico City

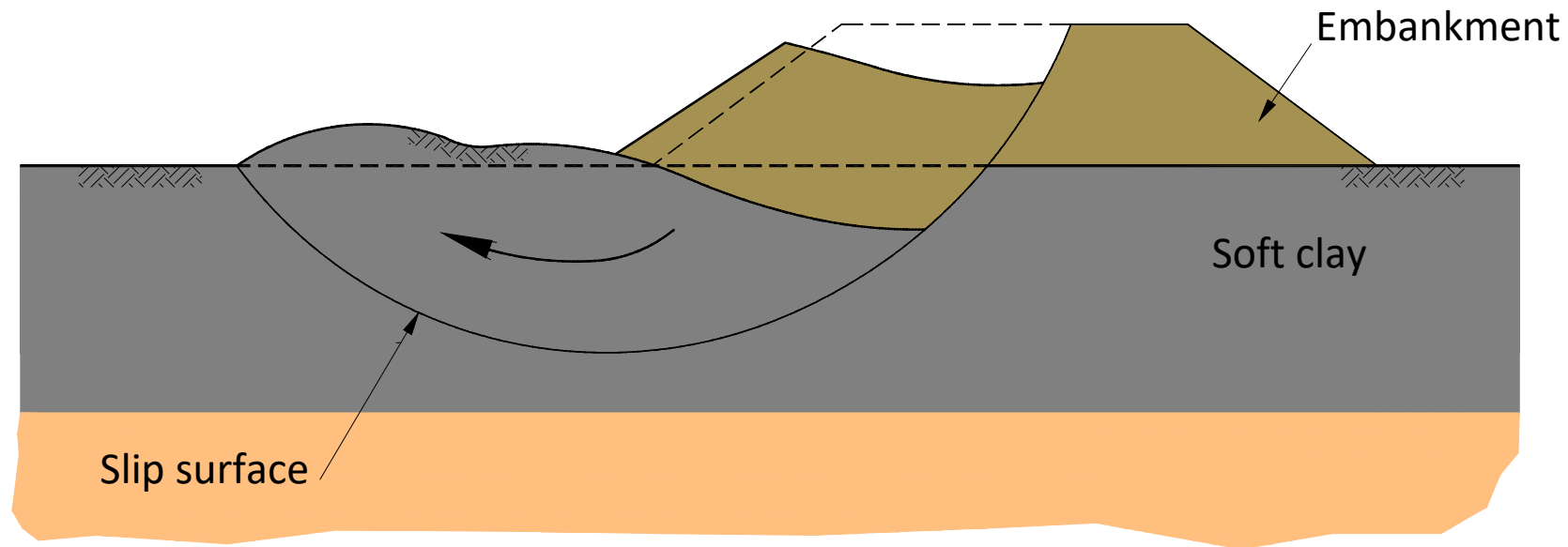
Courtesy of Sociedad Mexicana de Mecanica de Suelos

If a static load is applied on a clay whose water content is close to  $w_L$ , what can be expected?



Large delayed settlements due to reduction of the water content.

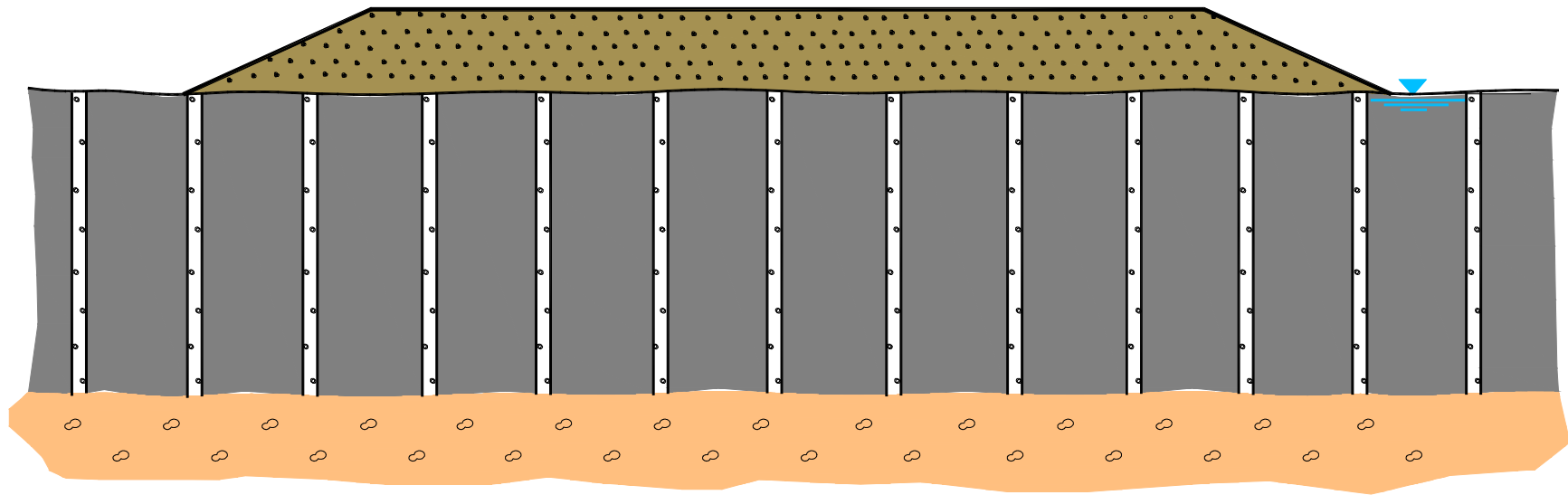
**If a static load is applied on a clay whose water content is close to  $w_L$  what can be expected?**



**... or even a slip failure involving the soft clay and the embankment.**



# How can we prevent such poor performance?



Settlement acceleration - vertical drains  
Soil reinforcement – stone columns

## SIMPLE, ESSENTIAL, BUT OFTEN OMITTED QUESTIONS!

- **Where is the clay just after the sedimentation?**
- How does Nature improve clayey soils?
- What are the consequences of such reduction to the response to static loading?
- If we apply a static load on a clay whose water content is close to  $w_L$ , what can we expect?
- How can we prevent such poor performance?
- **If at a given site we have two clayey layers, how can we compare their consistency index?**

## **SIMPLE, FUNDAMENTAL, but OFTEN OMITTED IDEAS!**

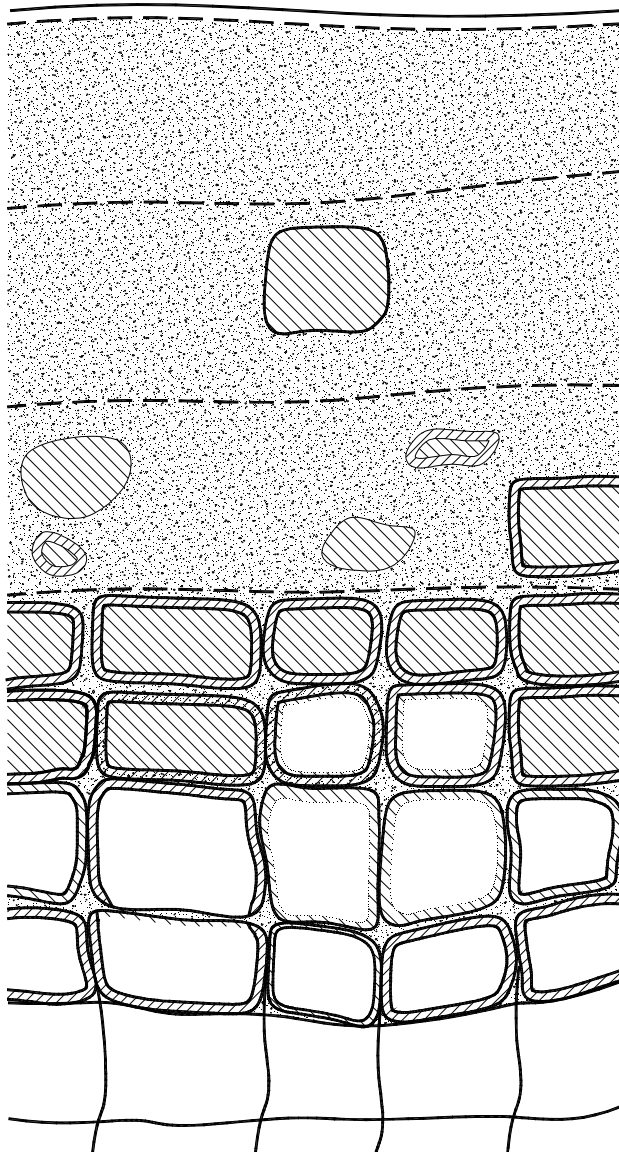
- Sedimentary soils are born in Nature very weak (loose/soft).
- They become stronger over time.
- Aged soils are typically sound soils.

## THIS HAS AN OBVIOUS RELATION WITH GEOLOGICAL PERIODS/EPOCHS

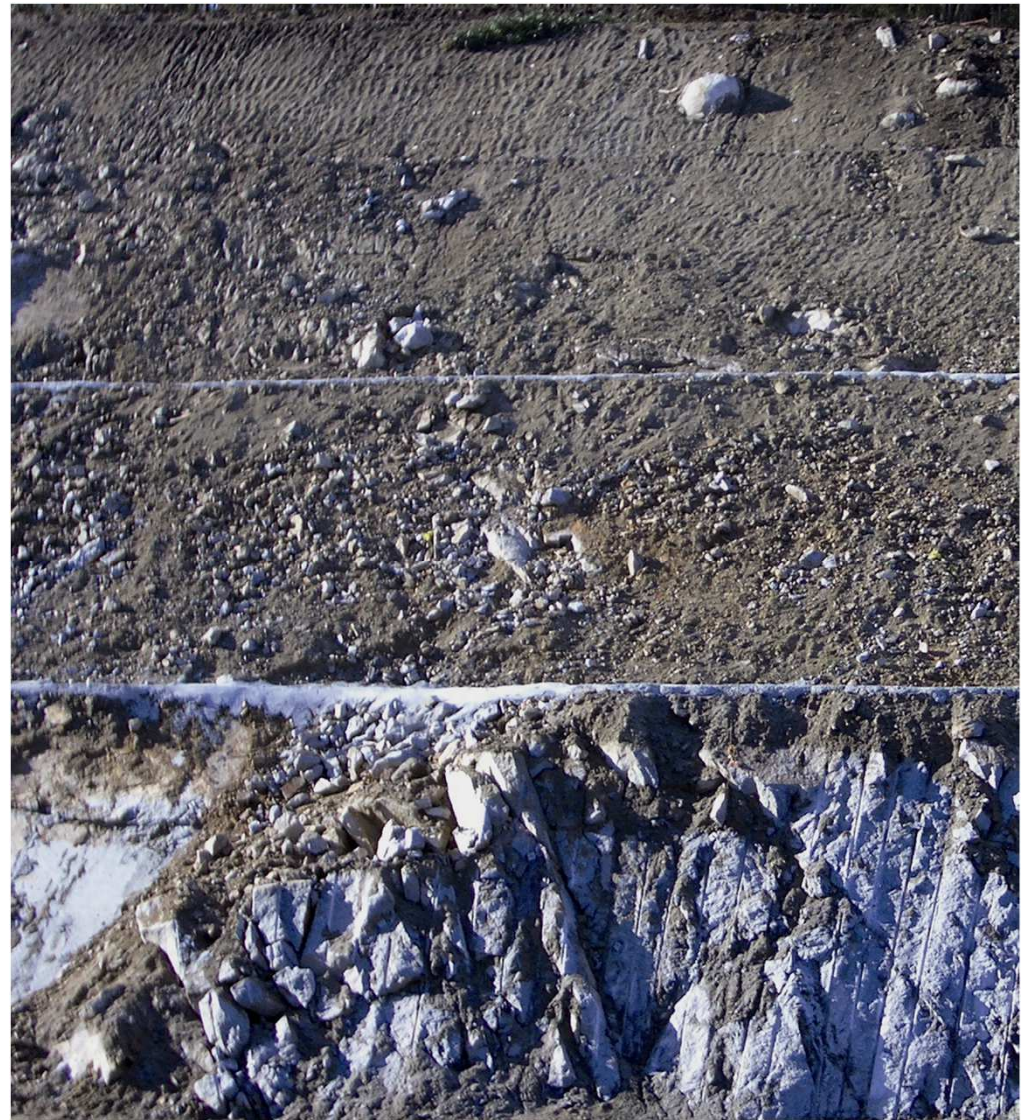
- a **Holocene** clay is certainly a soft clay.
- a **Holocene** sand is probably a loose sand.
- a **Pliocene** sand is likely a dense sand.
- a **Eocene** clay is surely a stiff/ hard clay.

In Nature, relations between Geology and  
Mechanics are fecund!

# Residual soils from granite (saprolite)



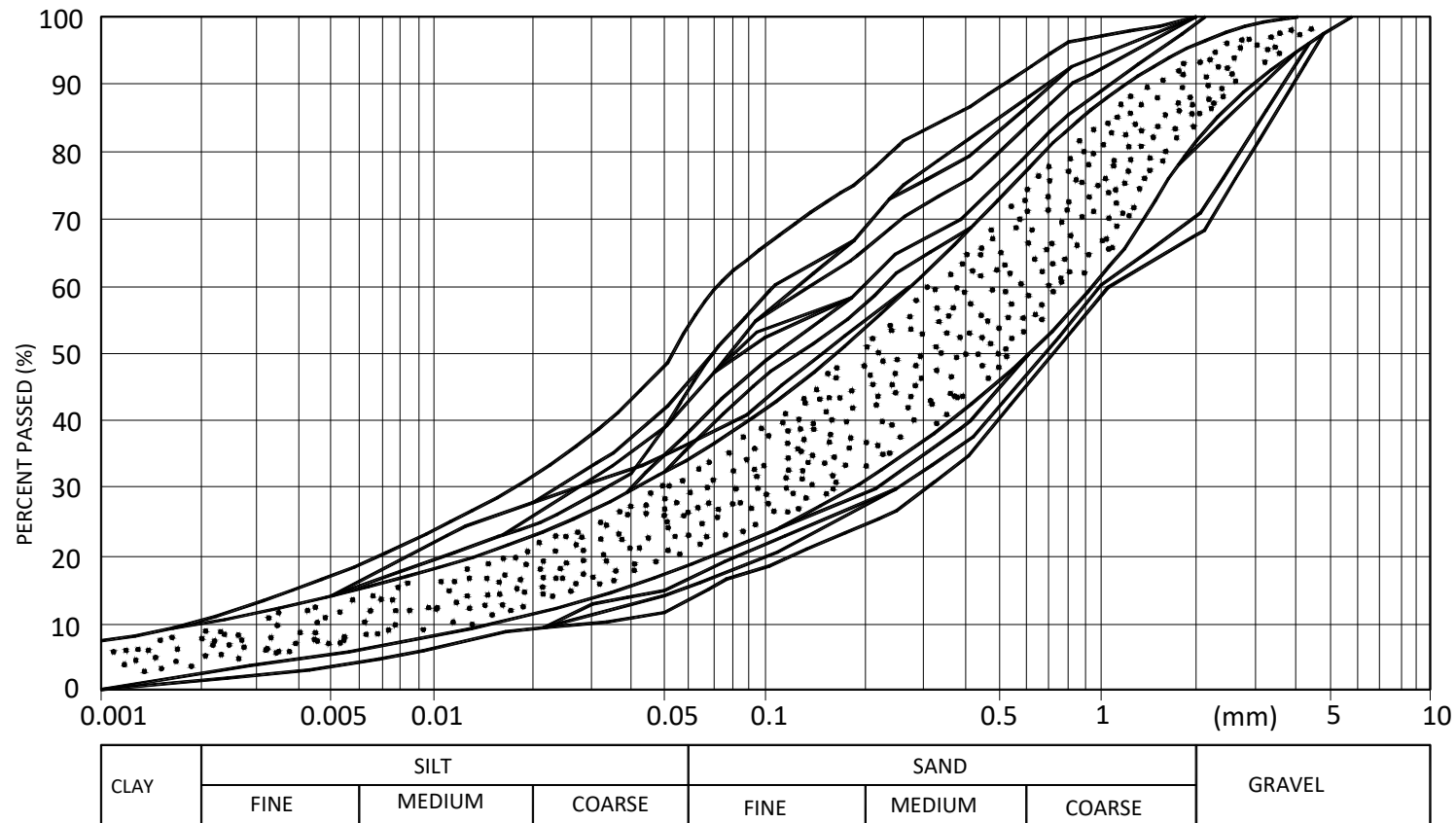
Little, 1969



Weathering profile in northern Portugal

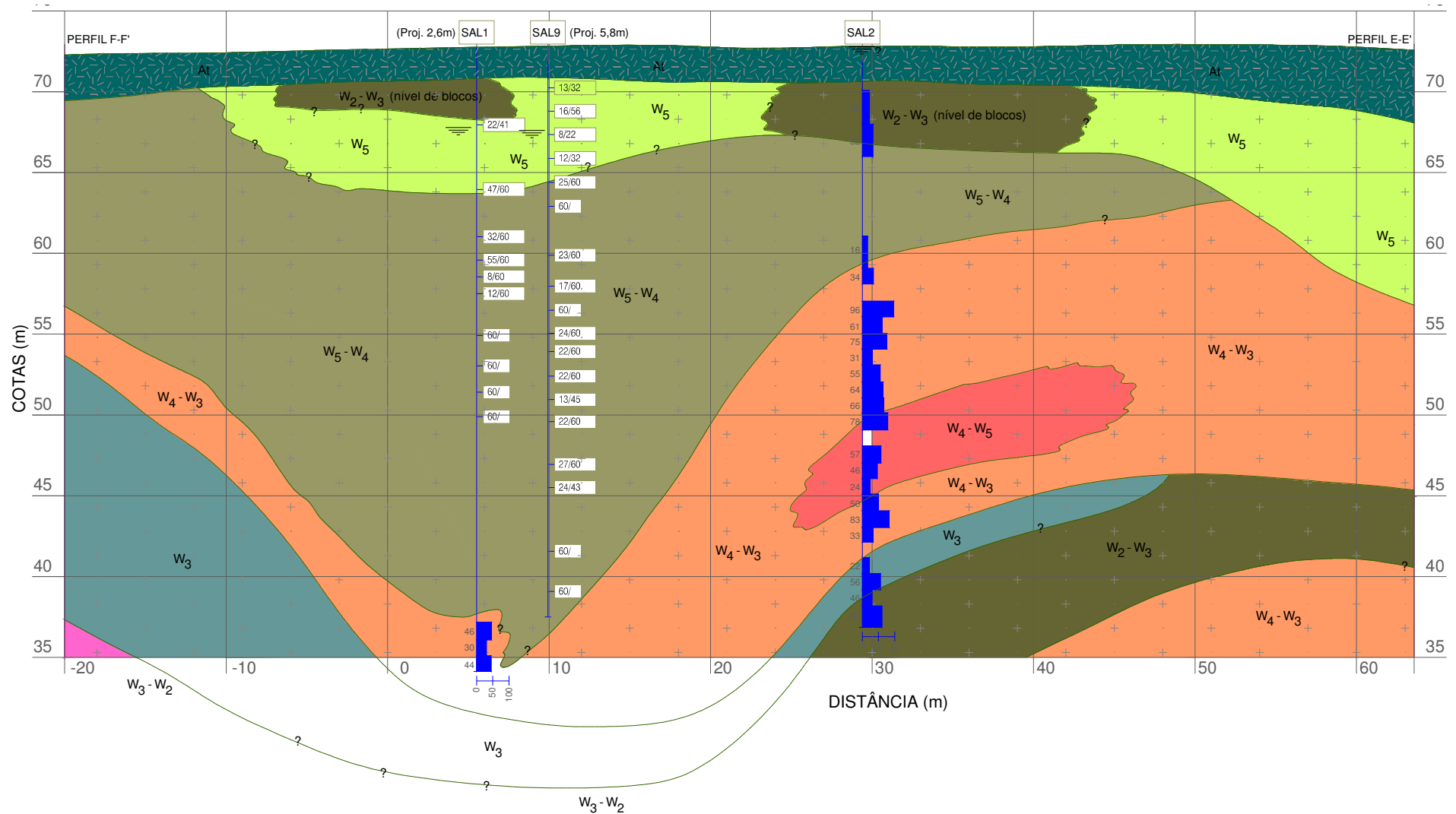


# Residual soils from granite (saprolite)



$\gamma_s$ (kN/m <sup>3</sup> )	$w_L$ (%)	$I_P$ (%)	$w$ (%)	$S_r$ (%)	$e$	$\gamma$ (kN/m <sup>3</sup> )
25.5 – 26.7	25 - 40	< 13	10 - 30	60 - 100	0.40 – 0.85	17.0 – 22.0

# Granite residual soils – typical heterogeneity



Av. Aliados, Porto, Portugal

Courtesy of Metro do Porto

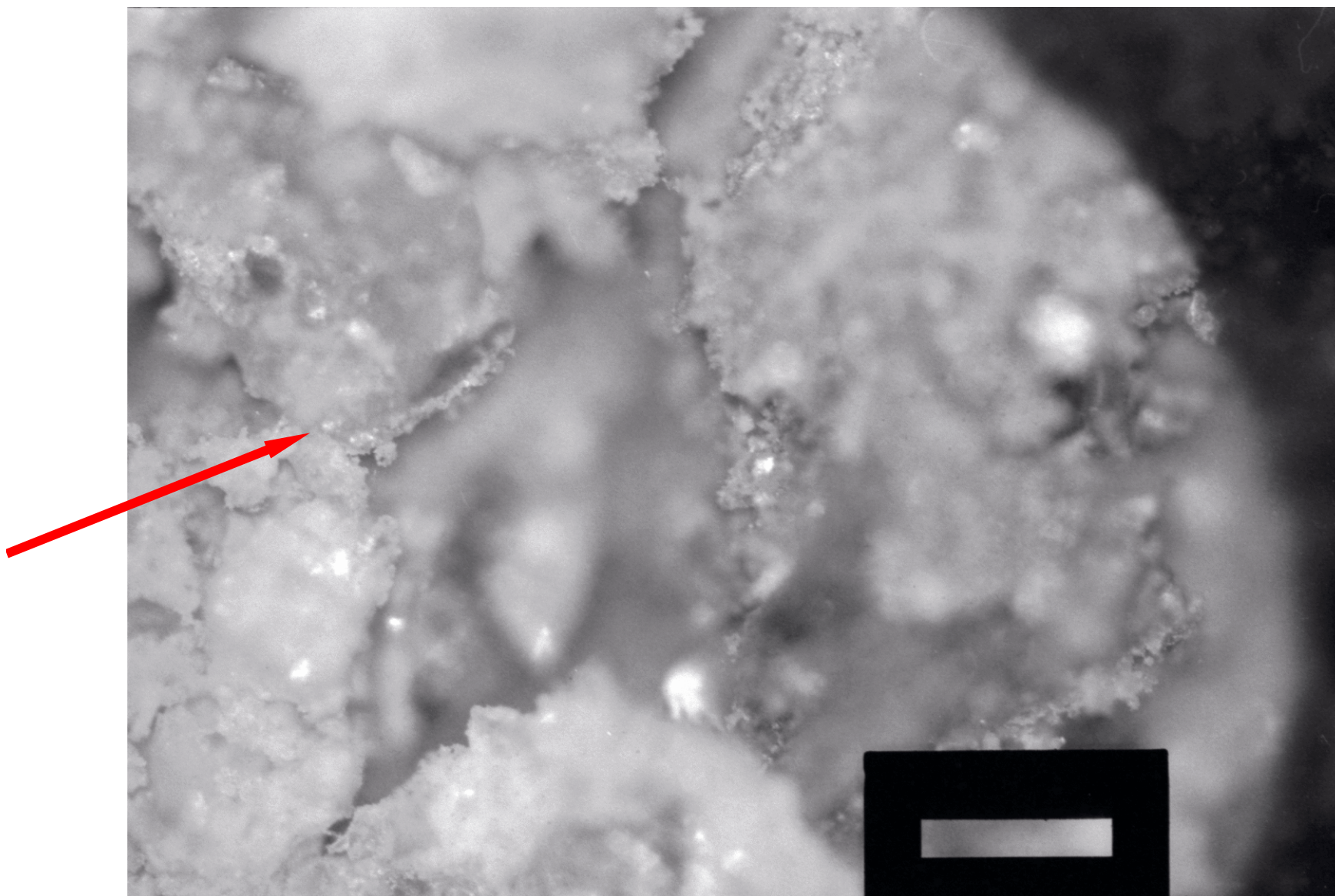


Photo by António Viana da Fonseca



# Granite saprolitic soils - relic structures



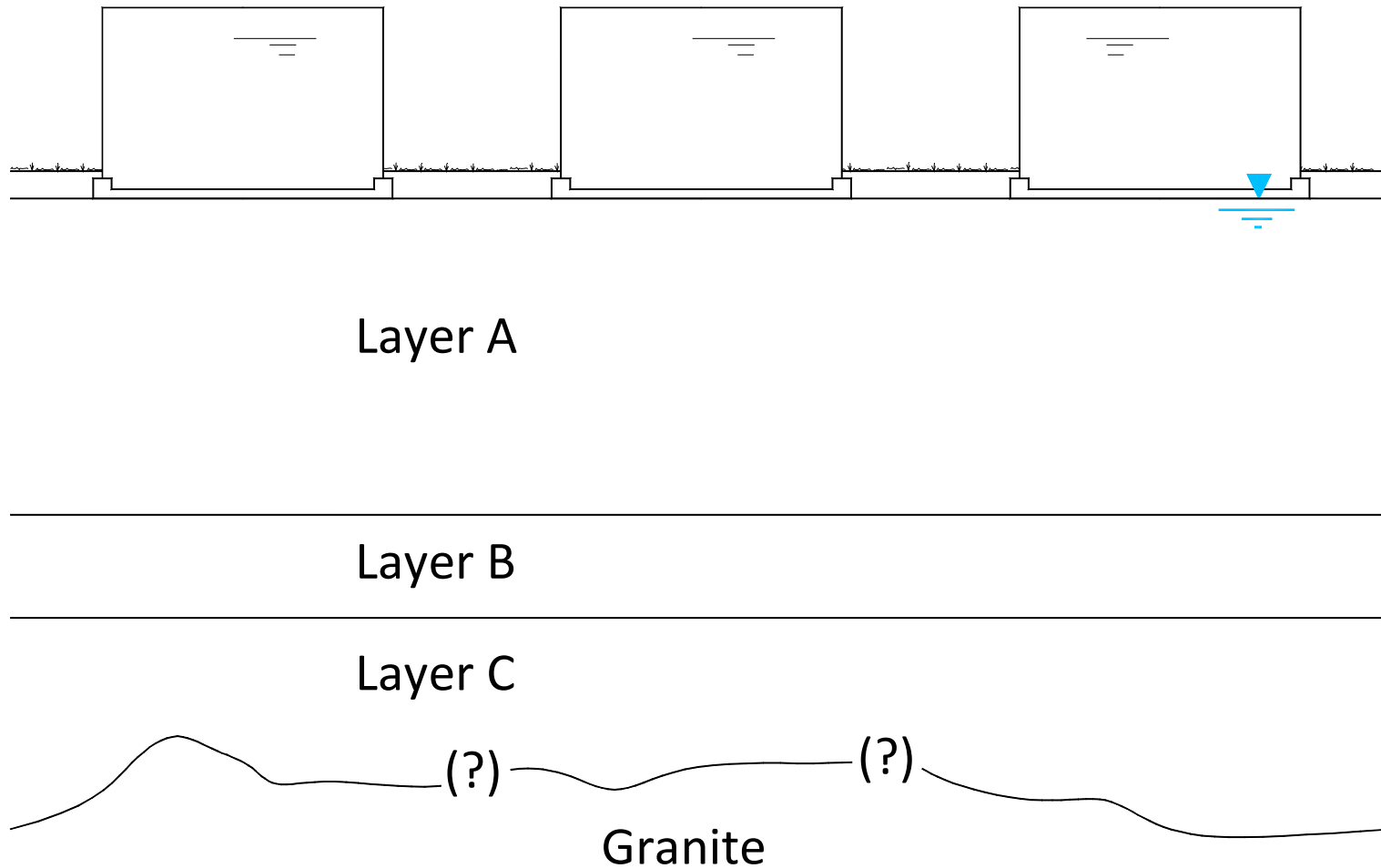
Photo by António Viana da Fonseca

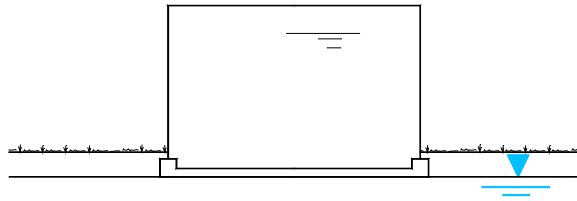
**Examples of exercises solved  
in weeks 3 and 4 of the semester.**

**This week (week 5) students are solving a  
short test with similar questions.**

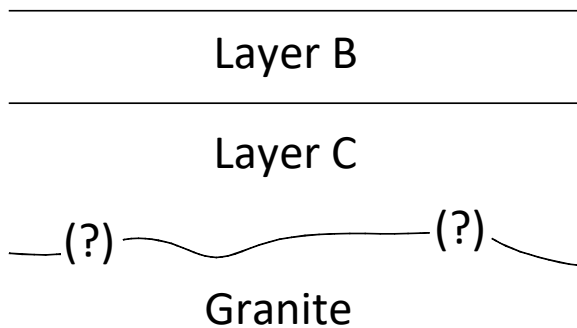


## Example 1: Cylindrical storage tank installation over sedimentary and residual soils on a granite substratum.

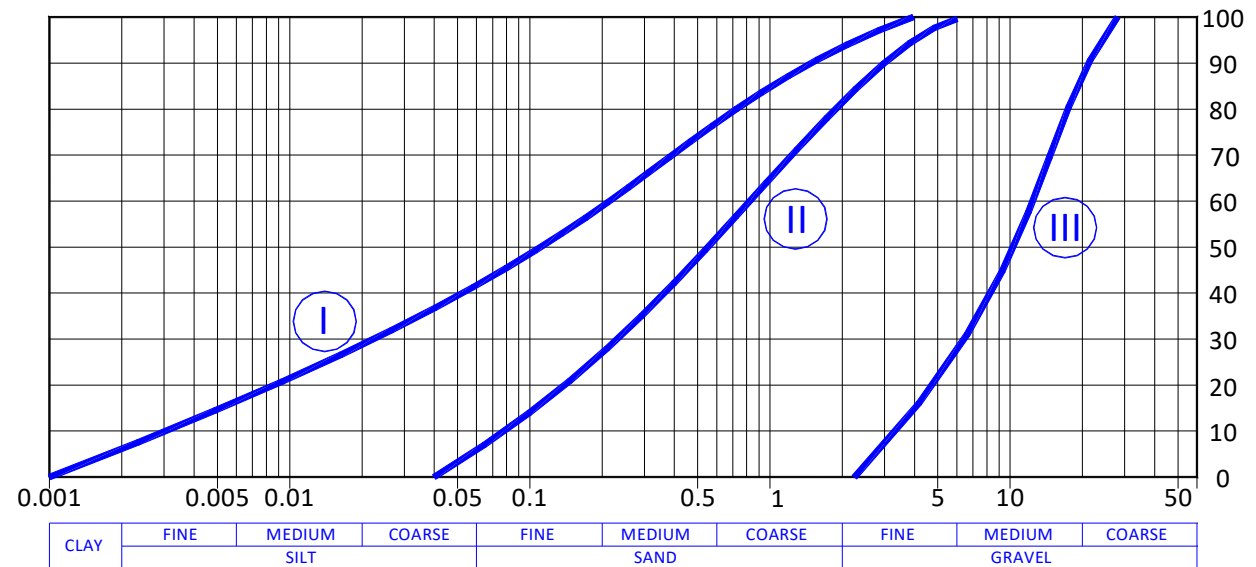




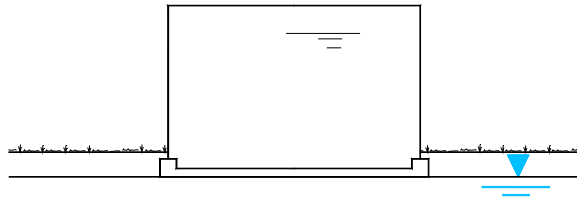
Layer A



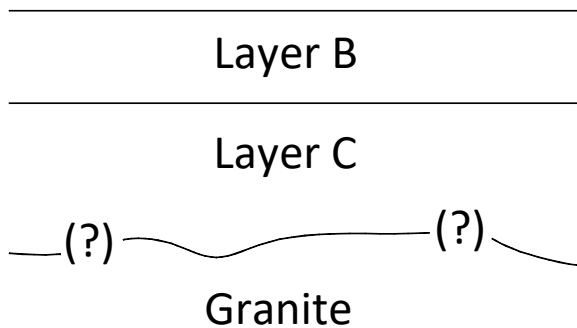
Soil	$w$ (%)	$\gamma_s$ (kN/m <sup>3</sup> )	$w_L$ (%)	$w_P$ (%)	$e_{min}$	$e_{max}$
1 (sedim.)	19	26.1	---	---	0.40	0.98
2 (residual)	23	25.8	34	25	---	---
3 (sedim.)	18	26.0	---	---	0.20	0.89



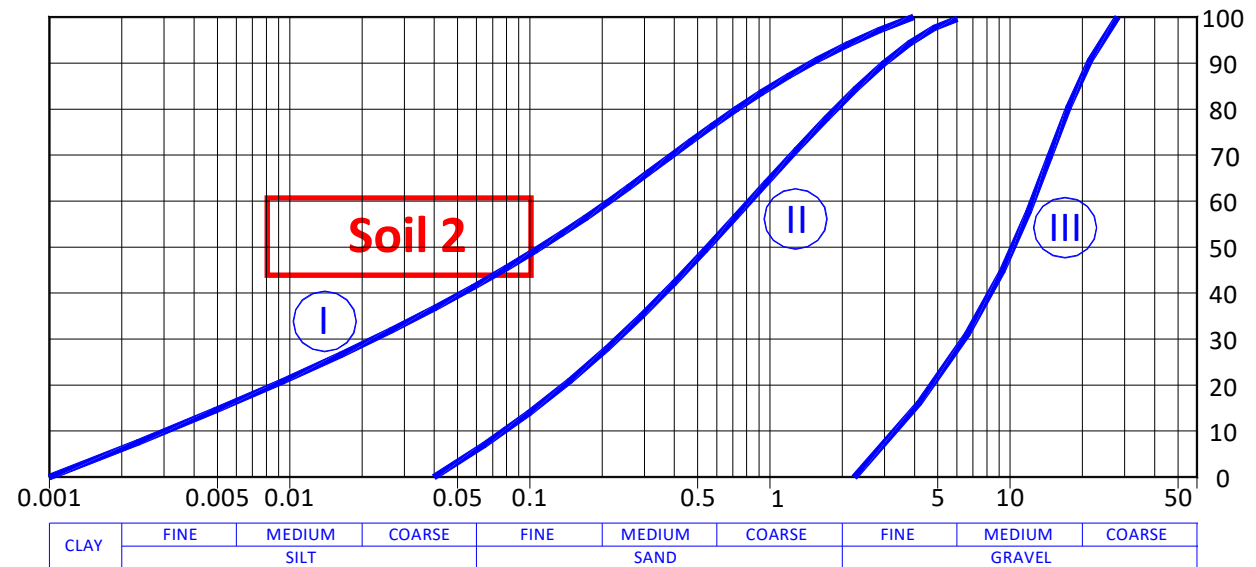
- Establish the most plausible correspondence between the soils of the table and the grain size curves.



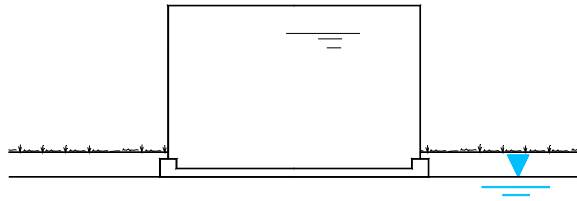
Layer A



Soil	w (%)	$\gamma_s$ (kN/m <sup>3</sup> )	w <sub>L</sub> (%)	w <sub>P</sub> (%)	e <sub>min</sub>	e <sub>max</sub>
1 (sedim.)	19	26.1	---	---	0.40	0.98
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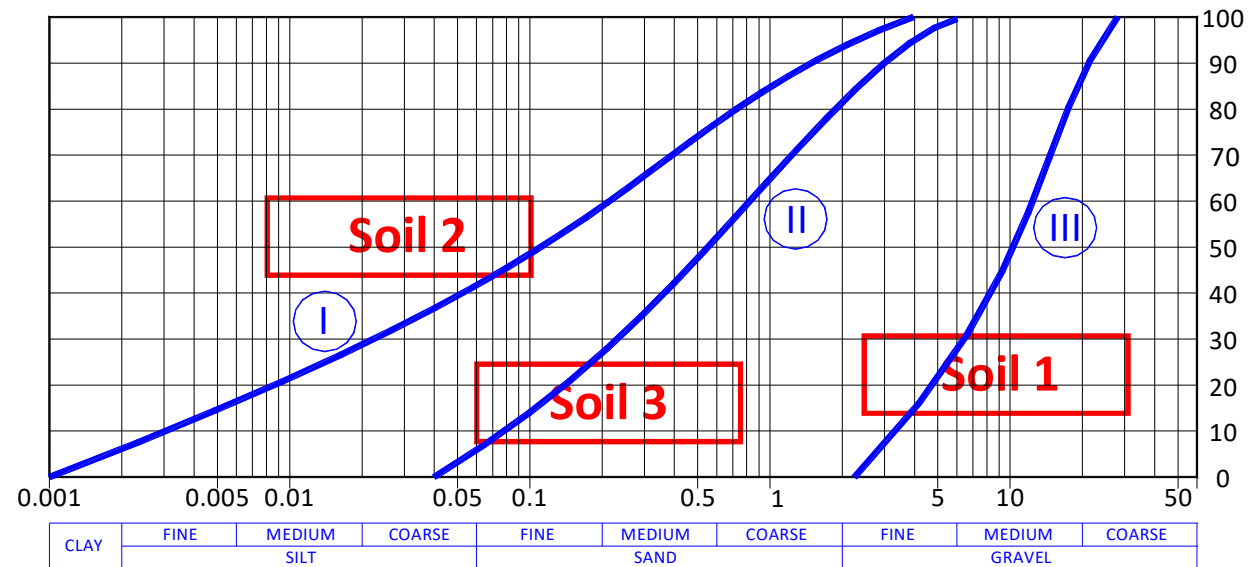
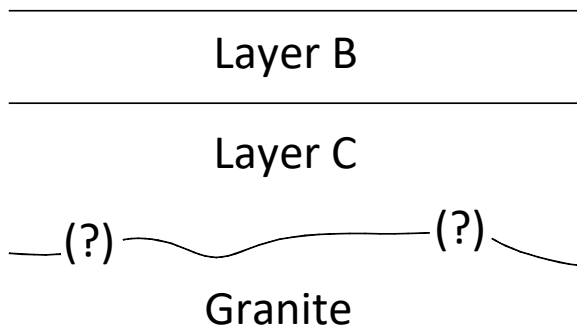


- Establish the most plausible correspondence between the soils of the table and the grain size curves.

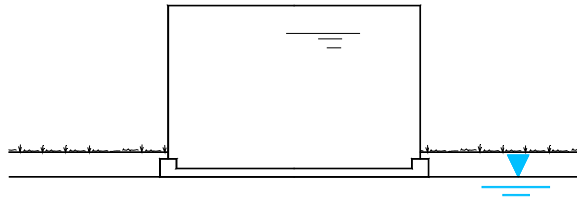


Layer A

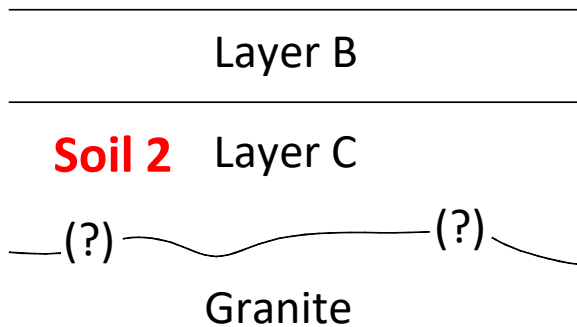
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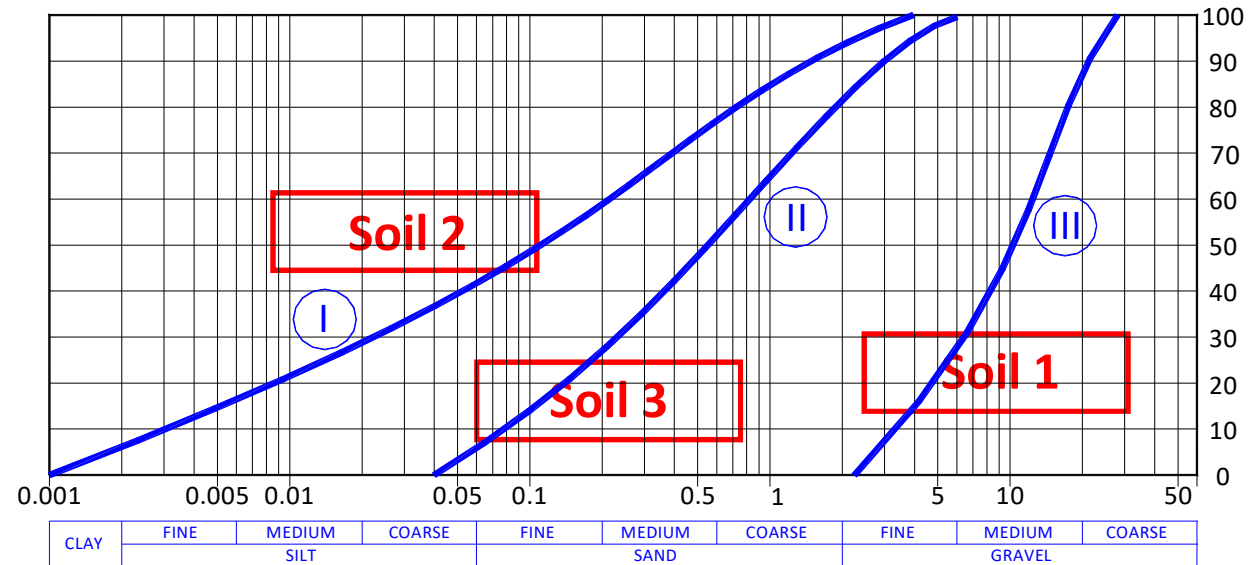
- Establish the most plausible correspondence between the soils of the table and the grain size curves.



Layer A

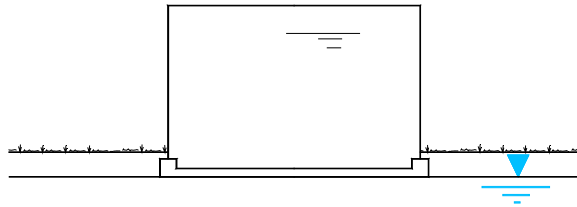


Soil	w (%)	$\gamma_s$ (kN/m <sup>3</sup> )	w <sub>L</sub> (%)	w <sub>P</sub> (%)	e <sub>min</sub>	e <sub>max</sub>
1 (sedim.)	19	26.1	---	---	0.40	0.98
2 (residual)	23	25.8	34	25	---	---
3 (sedim.)	18	26.0	---	---	0.20	0.89



- Establish the most plausible correspondence between layers A, B and C of the figure and soils of the table. Present the computations which justify your answer.





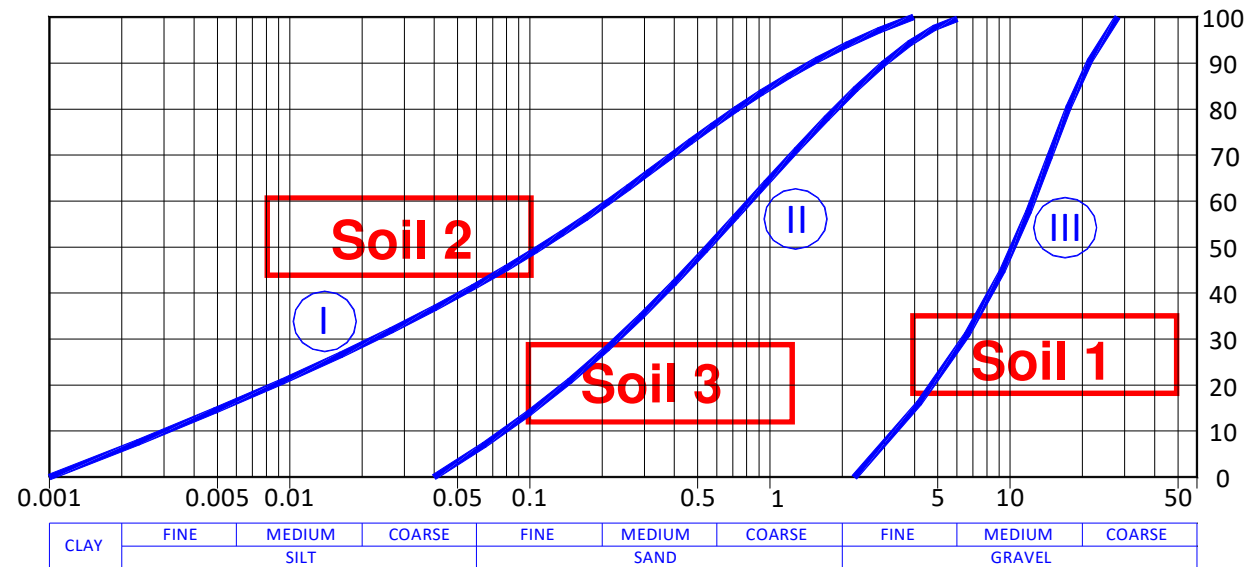
**Soil 3** Layer A

**Soil 1** Layer B

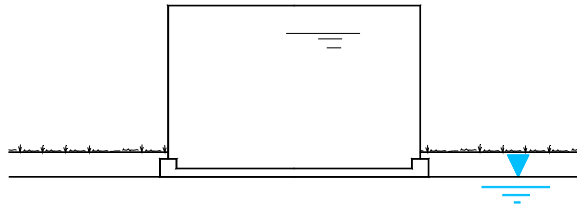
**Soil 2** Layer C



Soil	w (%)	$\gamma_s$ (kN/m <sup>3</sup> )	w <sub>L</sub> (%)	w <sub>p</sub> (%)	e <sub>min</sub>	e	e <sub>max</sub>
1 (sedim.)	19	26.1	---	---	0.40	0.51	0.98
2 (residual)	23	25.8	34	25	---	---	---
3 (sedim.)	18	26.0	---	---	0.20	0.74	0.89



- Establish the most plausible correspondence between layers A, B and C of the figure and soils of the table. Present the computations which justify your answer.

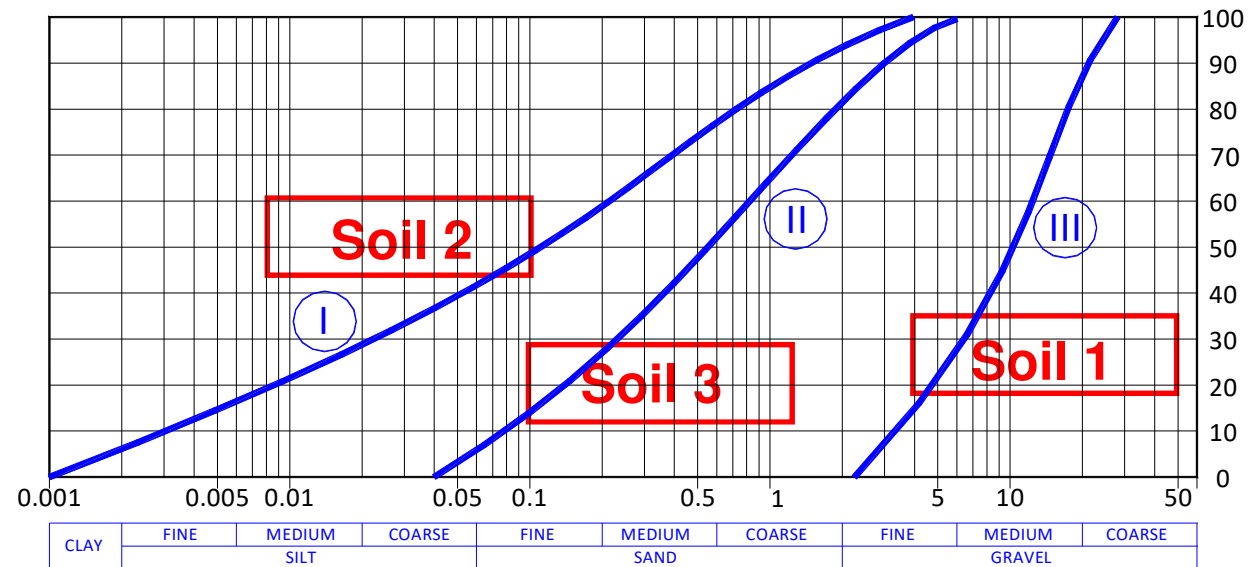


**Soil 3** Layer A

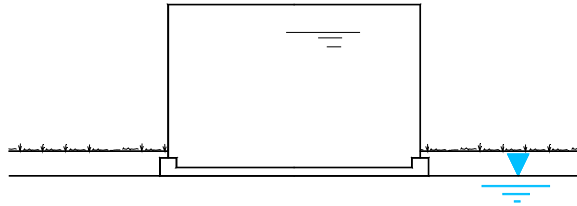
Soil	w (%)	$\gamma_s$ (kN/m <sup>3</sup> )	w <sub>L</sub> (%)	w <sub>p</sub> (%)	e <sub>min</sub>	e	e <sub>max</sub>
1 (sedim.)	19	26.1	---	---	0.40	0.51	0.98
2 (residual)	23	25.8	34	25	---	---	---
3 (sedim.)	18	26.0	---	---	0.20	0.74	0.89

**Soil 1** Layer B

**Soil 2** Layer C



- In case of a strong earthquake, is it probable that one (or more) layer(s) exhibit poor performance? If that is the case, describe what may happen. Propose a method that can prevent it.



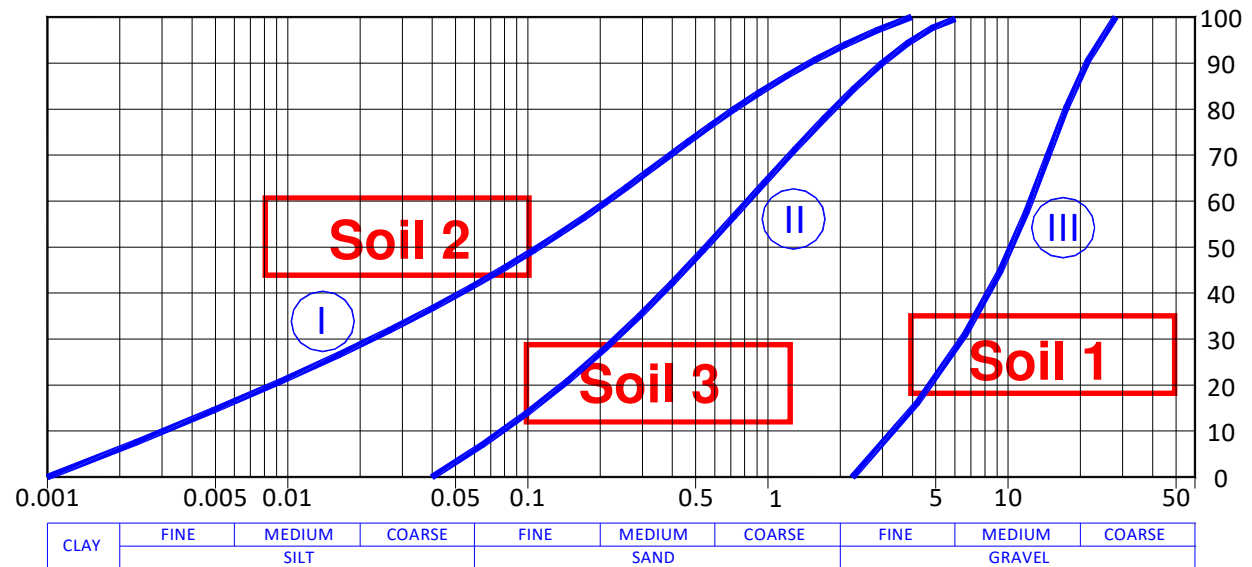
**Soil 3** Layer A

**Soil 1** Layer B

**Soil 2** Layer C

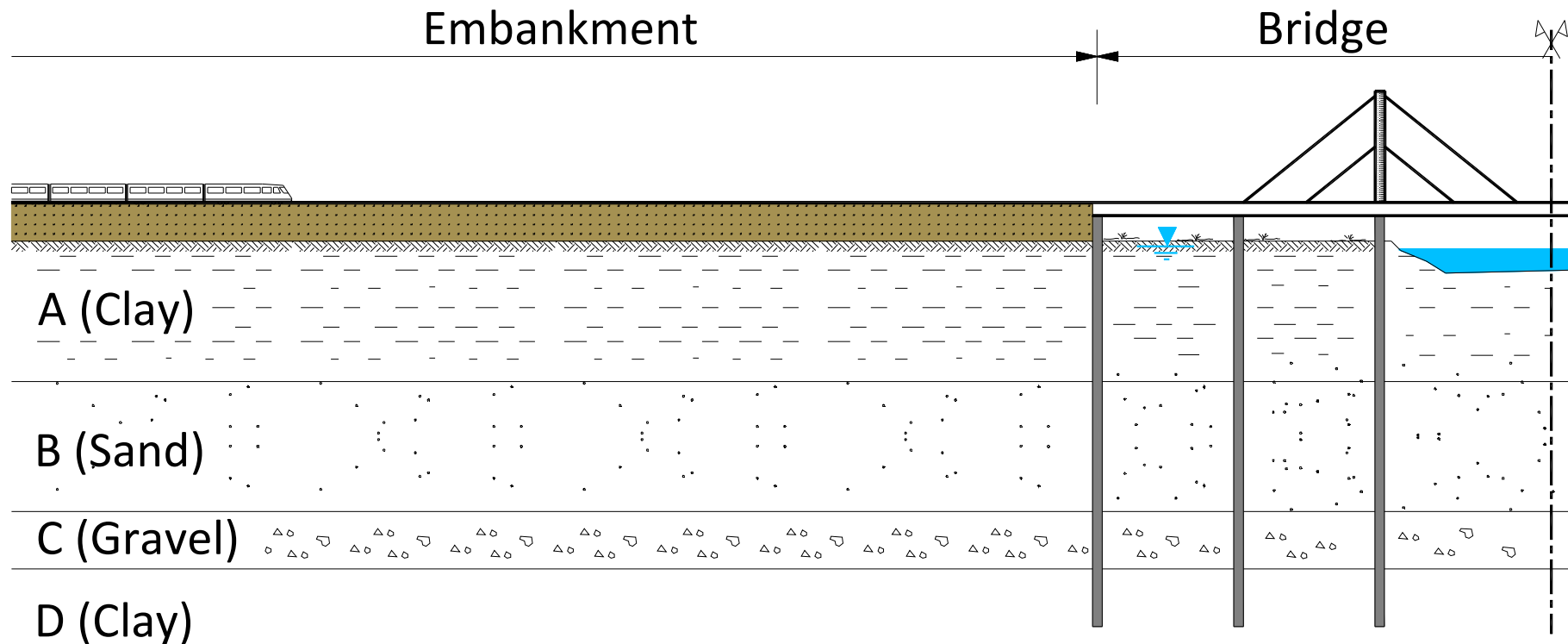
(?) (?)  
Granite

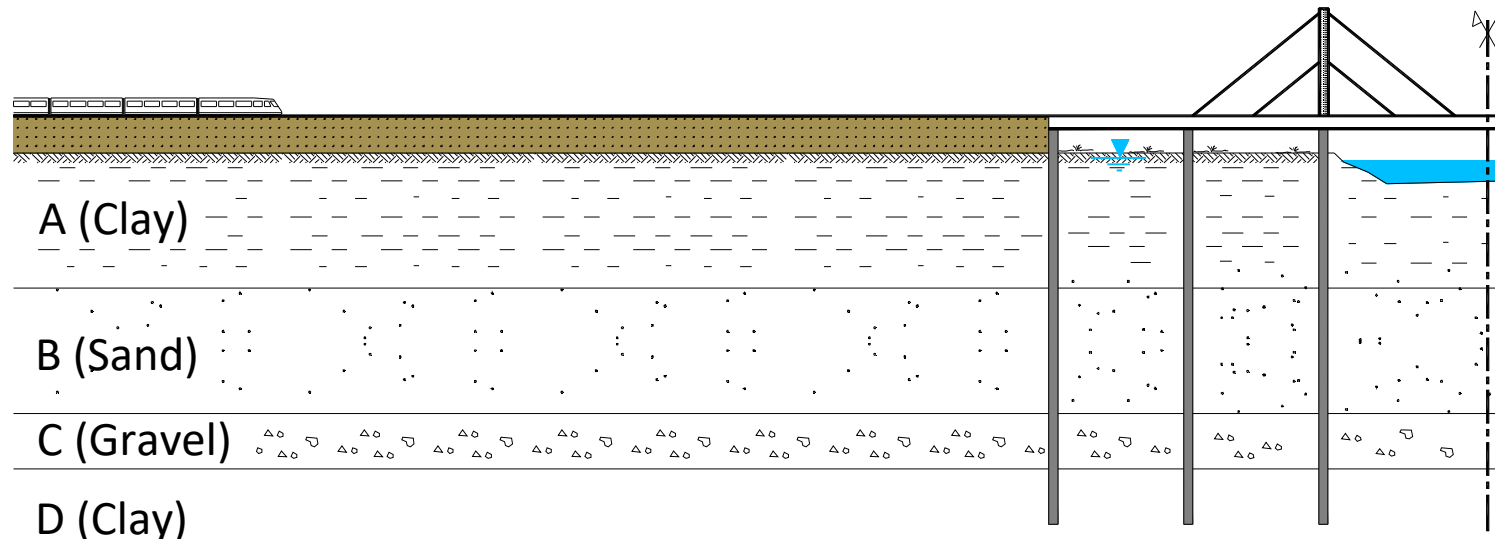
Soil	w (%)	$\gamma_s$ (kN/m <sup>3</sup> )	w <sub>L</sub> (%)	w <sub>p</sub> (%)	e <sub>min</sub>	e	e <sub>max</sub>
1 (sedim.)	19	26.1	---	---	0.40	0.51	0.98
2 (residual)	23	25.8	34	25	---	---	---
3 (sedim.)	18	26.0	---	---	0.20	0.74	0.89



- In case of a strong earthquake, is it probable that one (or more) layer(s) exhibit poor performance? If that is the case, describe what may happen. Propose a method that can prevent it.

## Example 2: crossing a wide alluvial plain by a new railway.

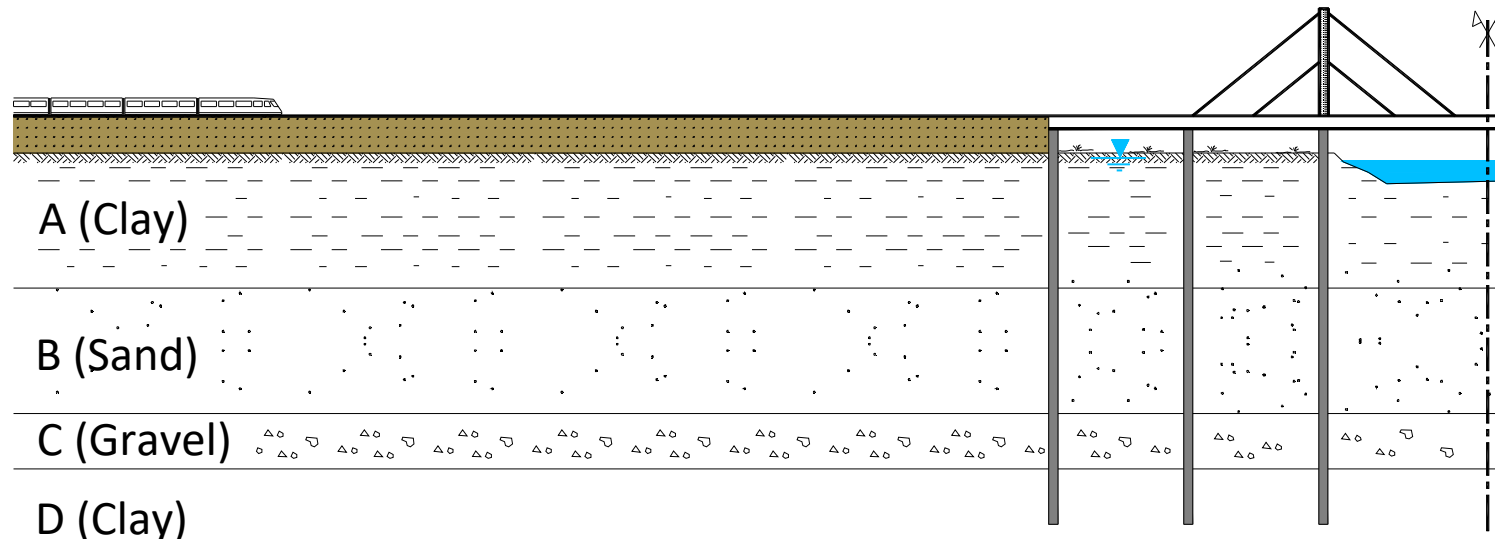




Soil	$\gamma_s$ (kN/m <sup>3</sup> )	$\gamma$ (kN/m <sup>3</sup> )	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e_{max}$
1	26.0	18.5	---	33	---	0.25	0.95
2	25.8	20.1	---	21	---	0.46	0.89
3	26.3	15.0	88	81	40	---	---
4	26.1	20.9	53	18	22	---	---

- Establish the most plausible correspondence between layers of the figure and the soils of the table.

Present the computations which justify your answer.

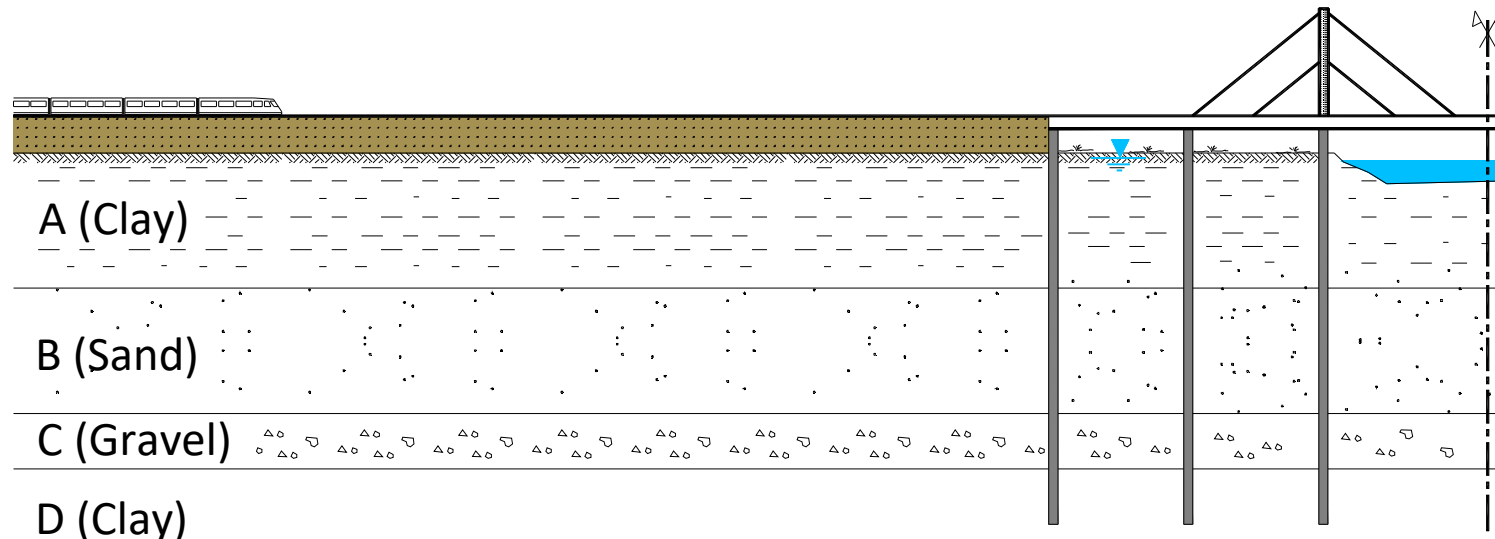


Soil	$\gamma_s$ (kN/m <sup>3</sup> )	$\gamma$ (kN/m <sup>3</sup> )	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$
1	26.0	18.5	---	33	---	0.25	0.87	0.95
2	25.8	20.1	---	21	---	0.46	0.55	0.89
3	26.3	15.0	88	81	40	---	2.17	---
4	26.1	20.9	53	18	22	---	0.48	---

- Establish the most plausible correspondence between layers of the figure and the soils of the table.

Present the computations which justify your answer.

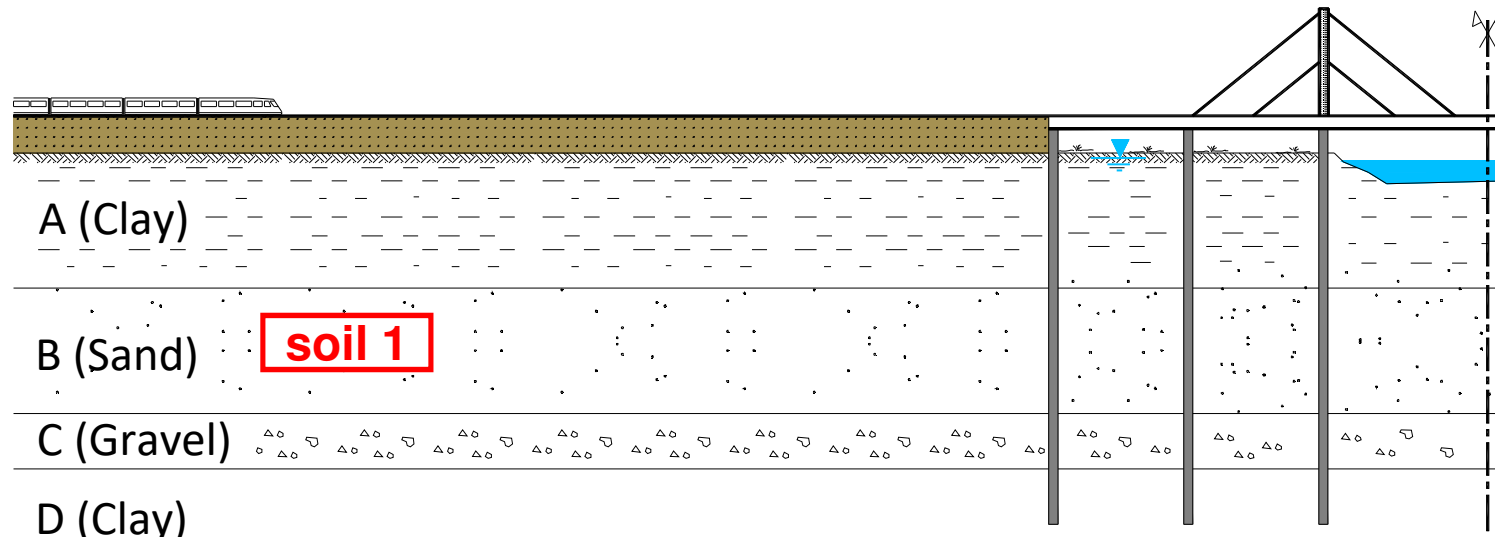




Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

- Establish the most plausible correspondence between layers of the figure and the soils of the table.

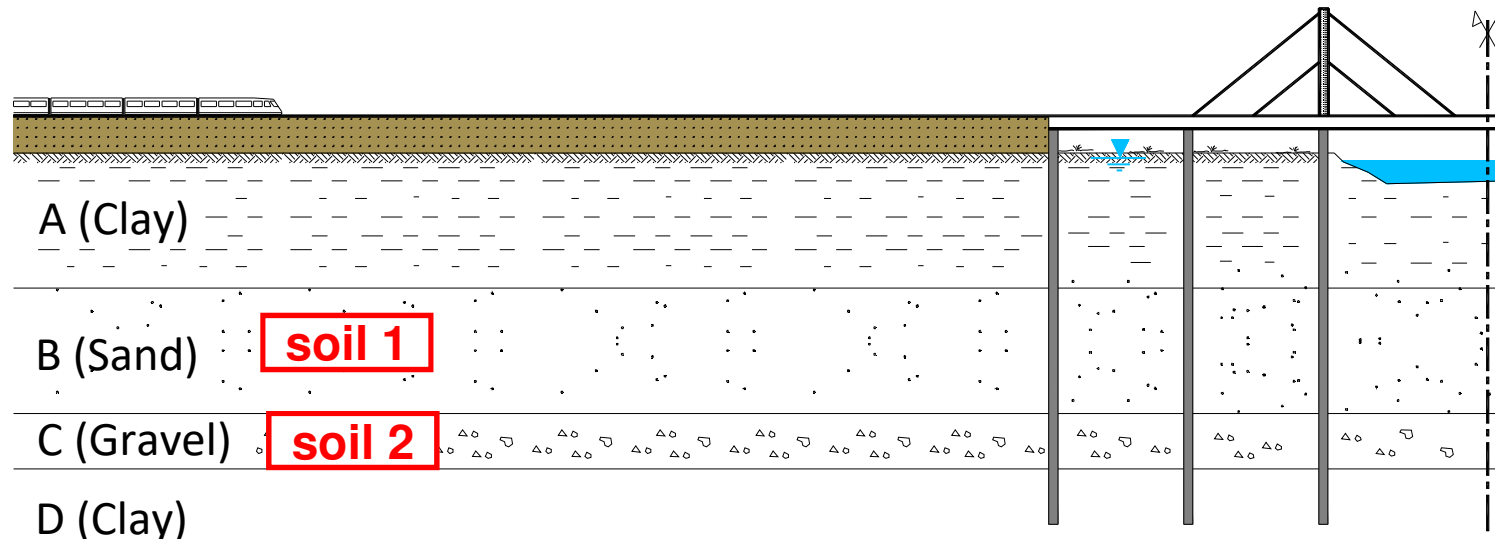
Present the computations which justify your answer.



Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

- Establish the most plausible correspondence between layers of the figure and the soils of the table.

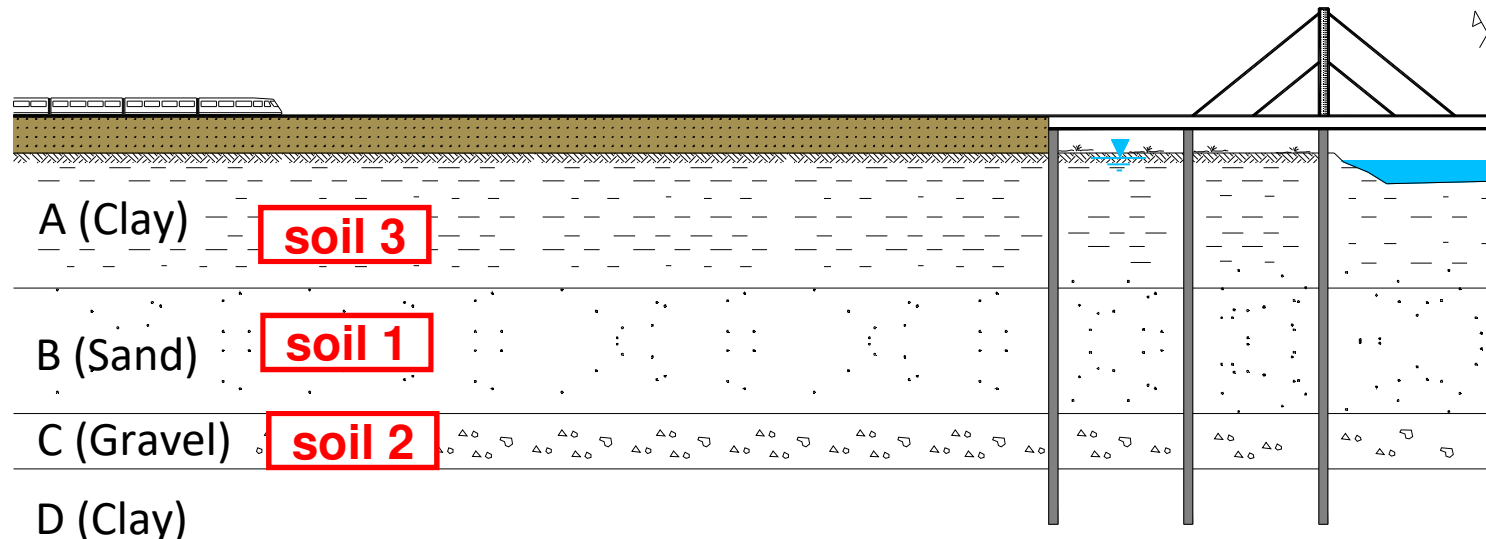
Present the computations which justify your answer.



Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{\min}$	$e$	$e_{\max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

- Establish the most plausible correspondence between layers of the figure and the soils of the table.

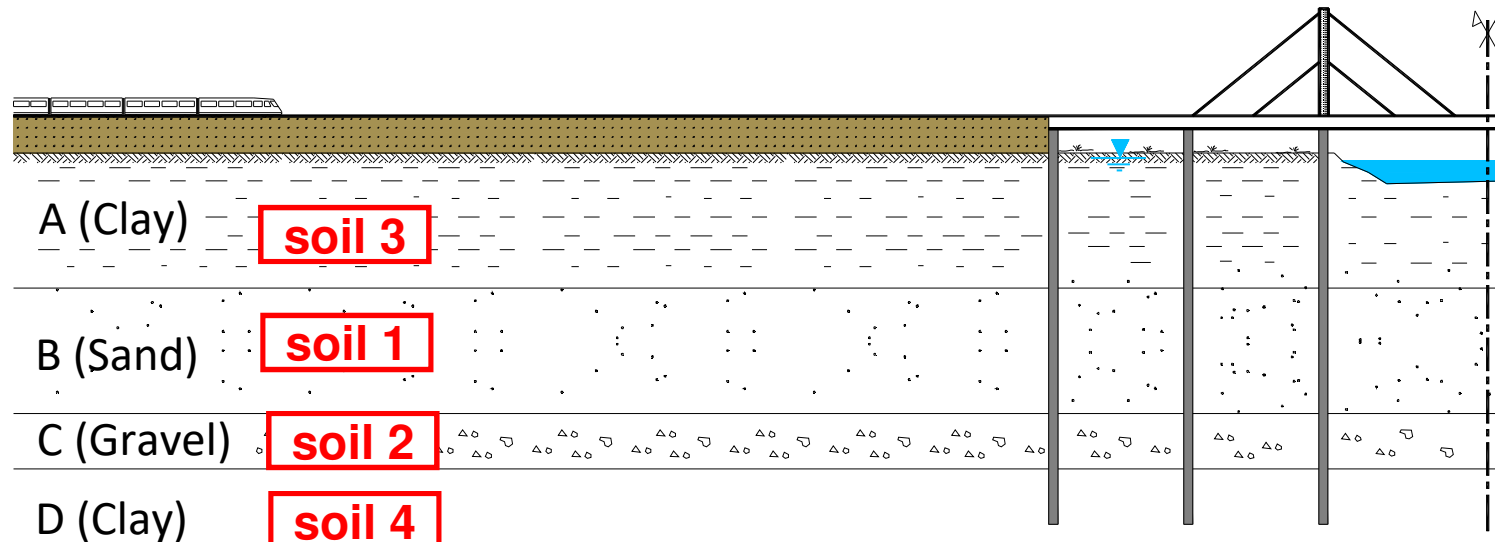
Present the computations which justify your answer.



Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

- Establish the most plausible correspondence between layers of the figure and the soils of the table.

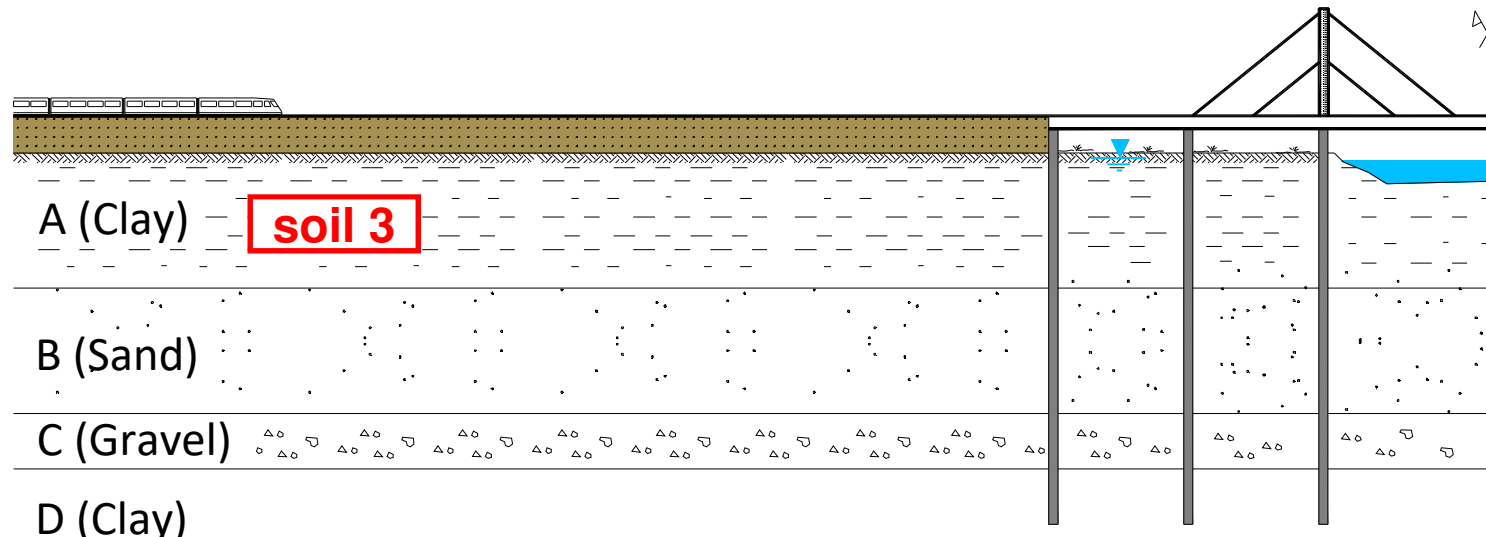
Present the computations which justify your answer.



Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

- Establish the most plausible correspondence between layers of the figure and the soils of the table.

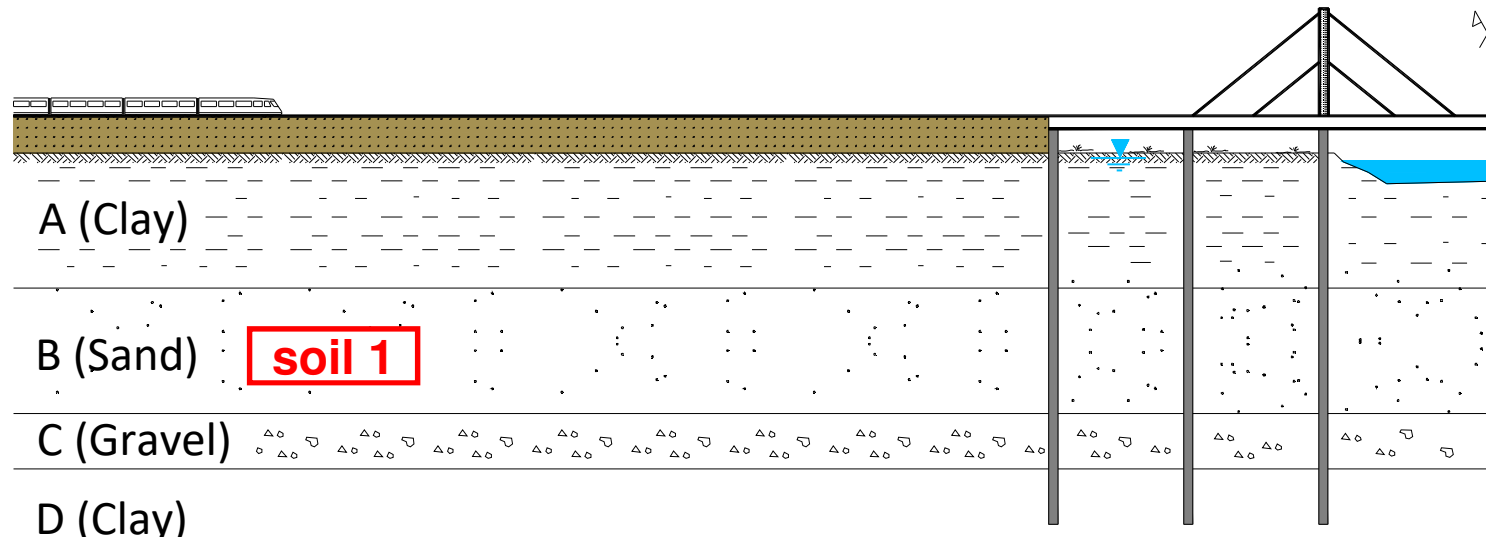
Present the computations which justify your answer.



Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

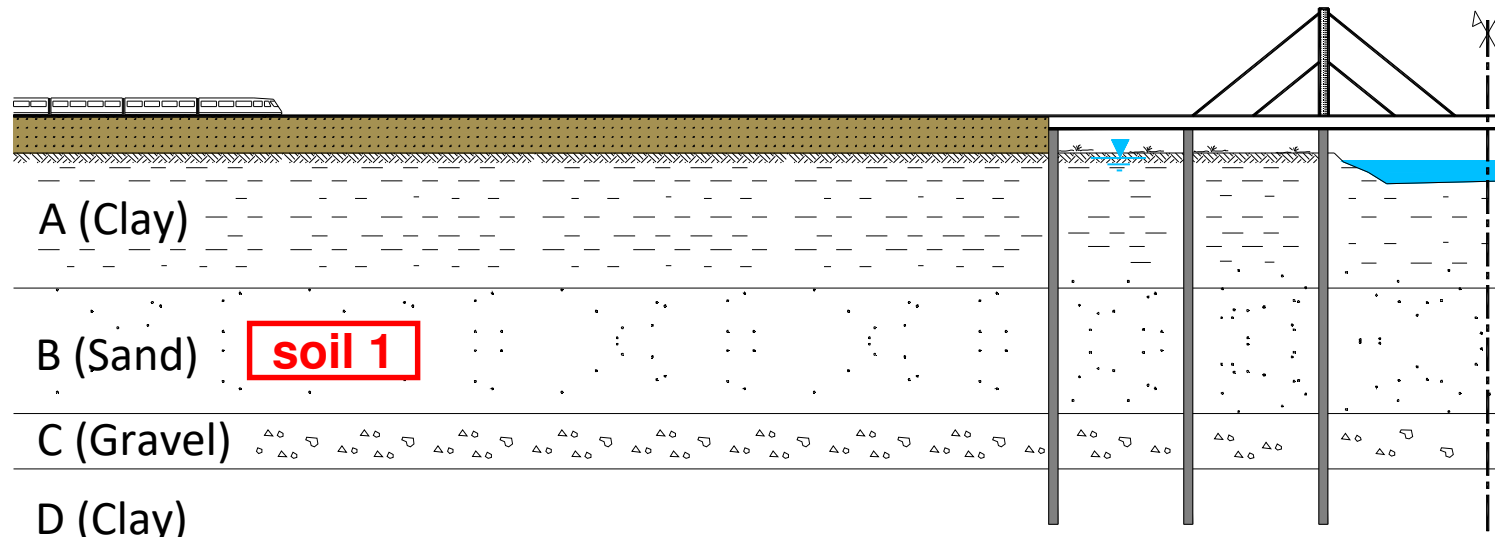
- Will any of the soils suffer large delayed settlements? If that is the case, identify the soil and propose a method for ensuring the settlement stabilization in a shorter time.





Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

- In case of a strong earthquake, is it probable that one (or more) layer(s) exhibit poor performance? If that is the case, describe what may happen. Propose a method that can prevent it.

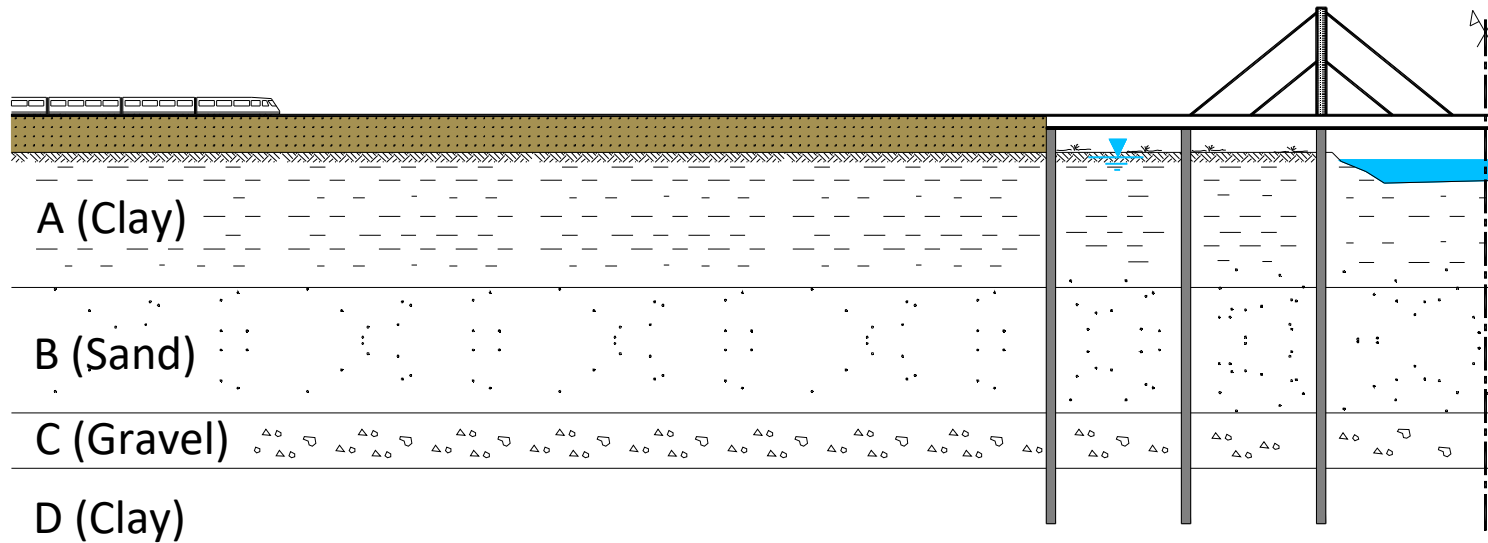


Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

- Which soil would you select (regardless its concrete position) as fill material for the embankment?

## OTHER POSSIBLE QUESTIONS (for the following weeks):

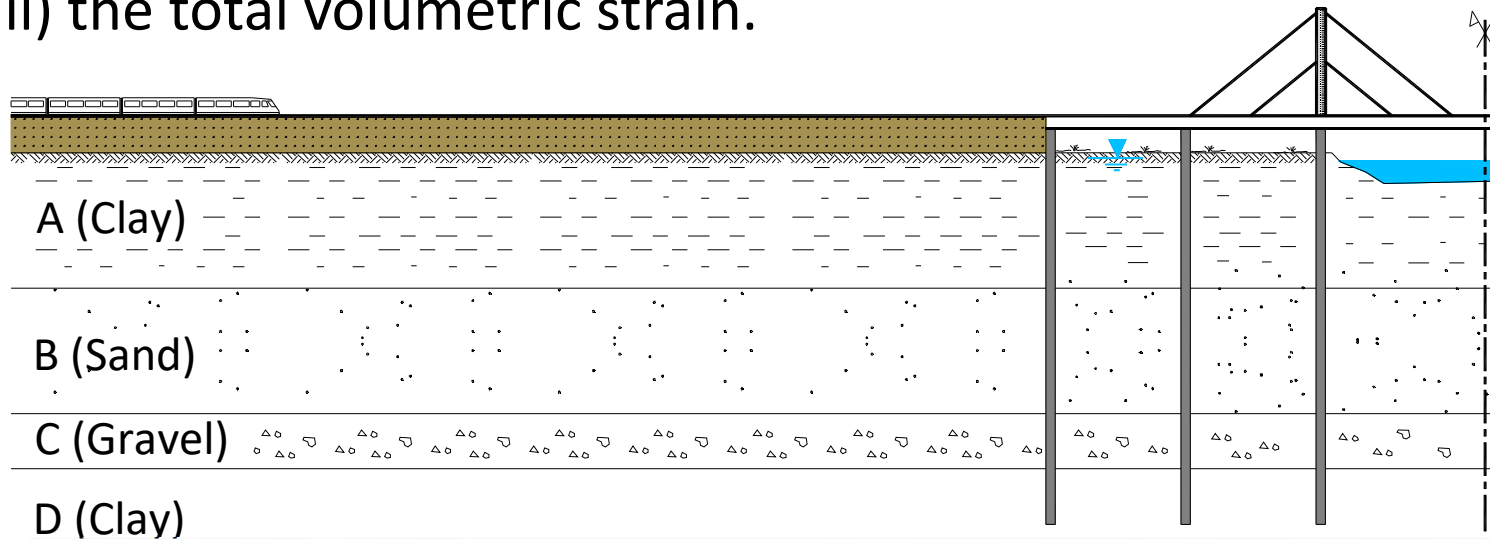
- Sort the soils in ascending order of permeability.



Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{\min}$	$e$	$e_{\max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

## OTHER POSSIBLE QUESTIONS (for the following weeks):

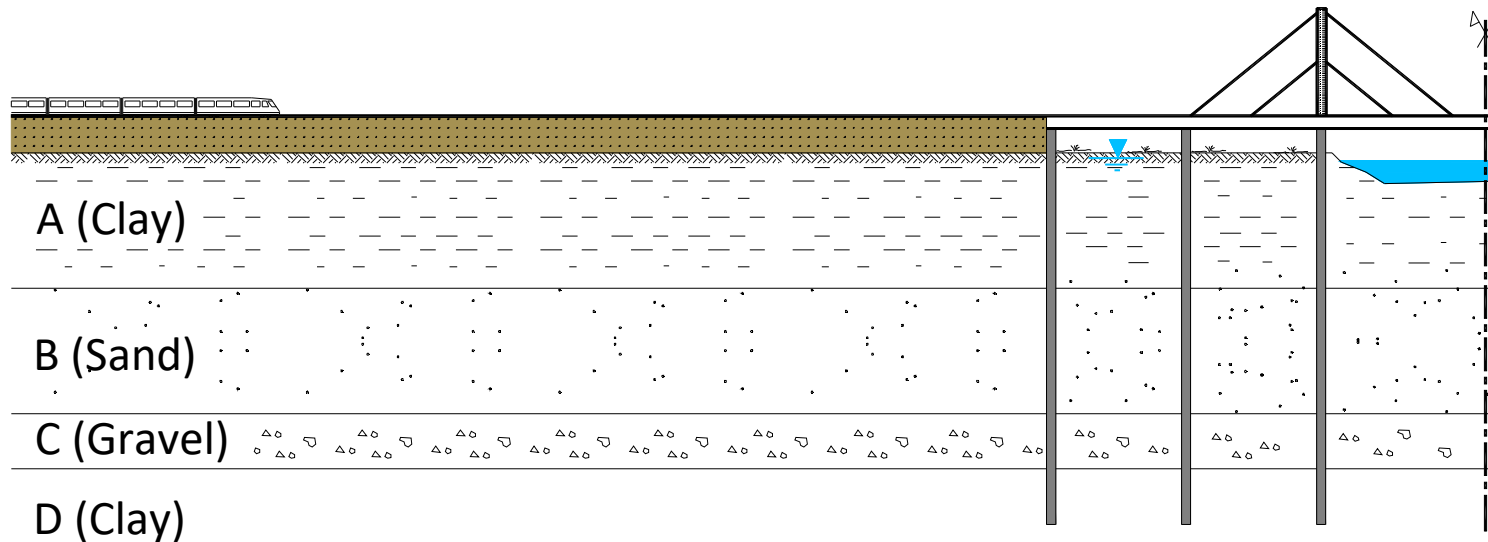
- Sort the soils in ascending order of compressibility, considering:
  - only immediate volumetric strain;
  - only time dependent volumetric strain;
  - the total volumetric strain.



Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

## OTHER POSSIBLE QUESTIONS (for the following weeks):

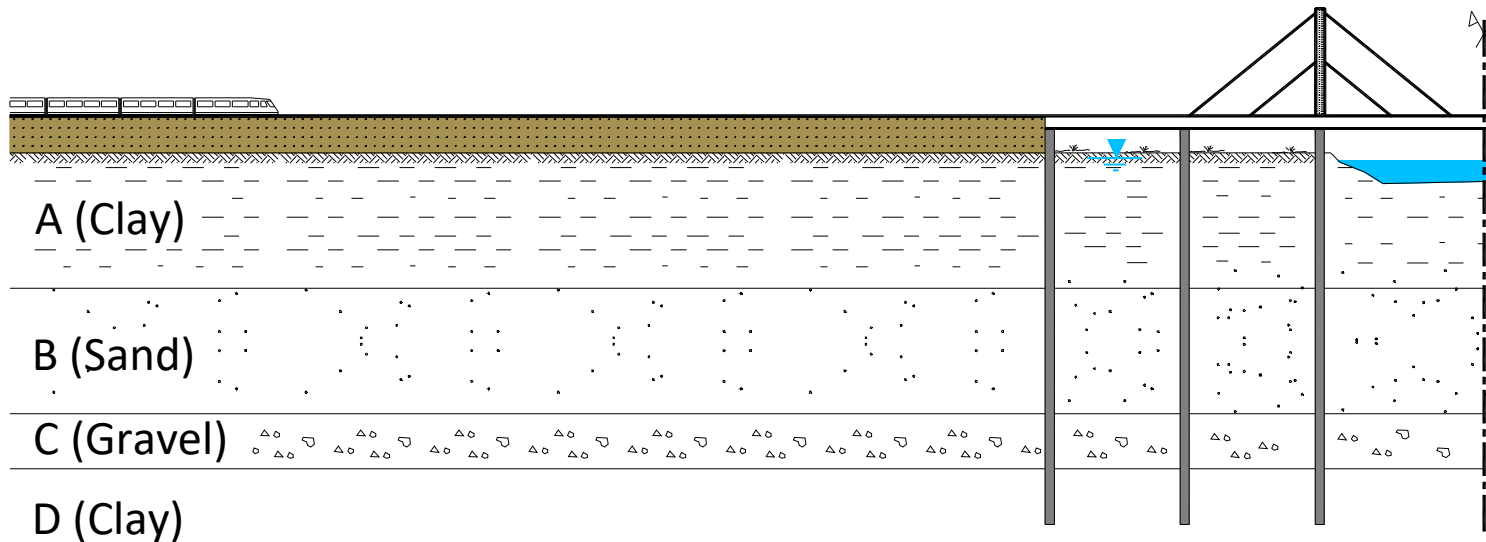
- Is any soil(s) to behave as a normally consolidated soil?
- Is any soil(s) to behave as an overconsolidated soil?



Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_C$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

## OTHER POSSIBLE QUESTIONS (for the following weeks):

- What would you say about the expected dilatancy (positive/negative) of the soils?

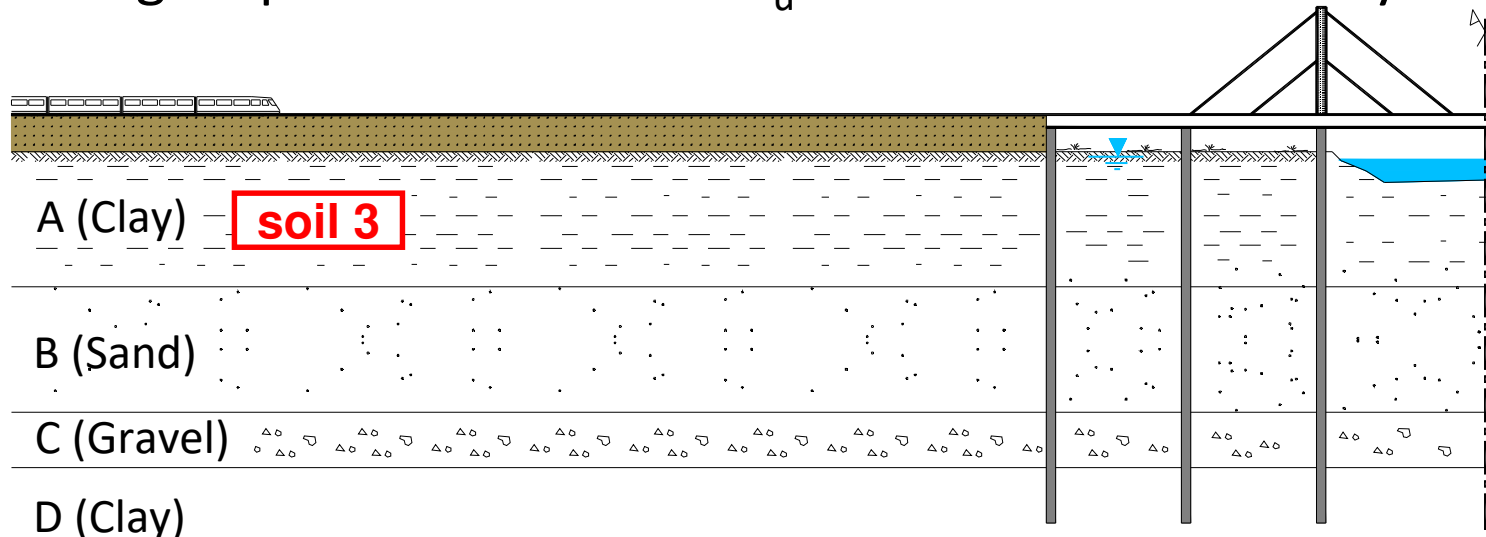


Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---



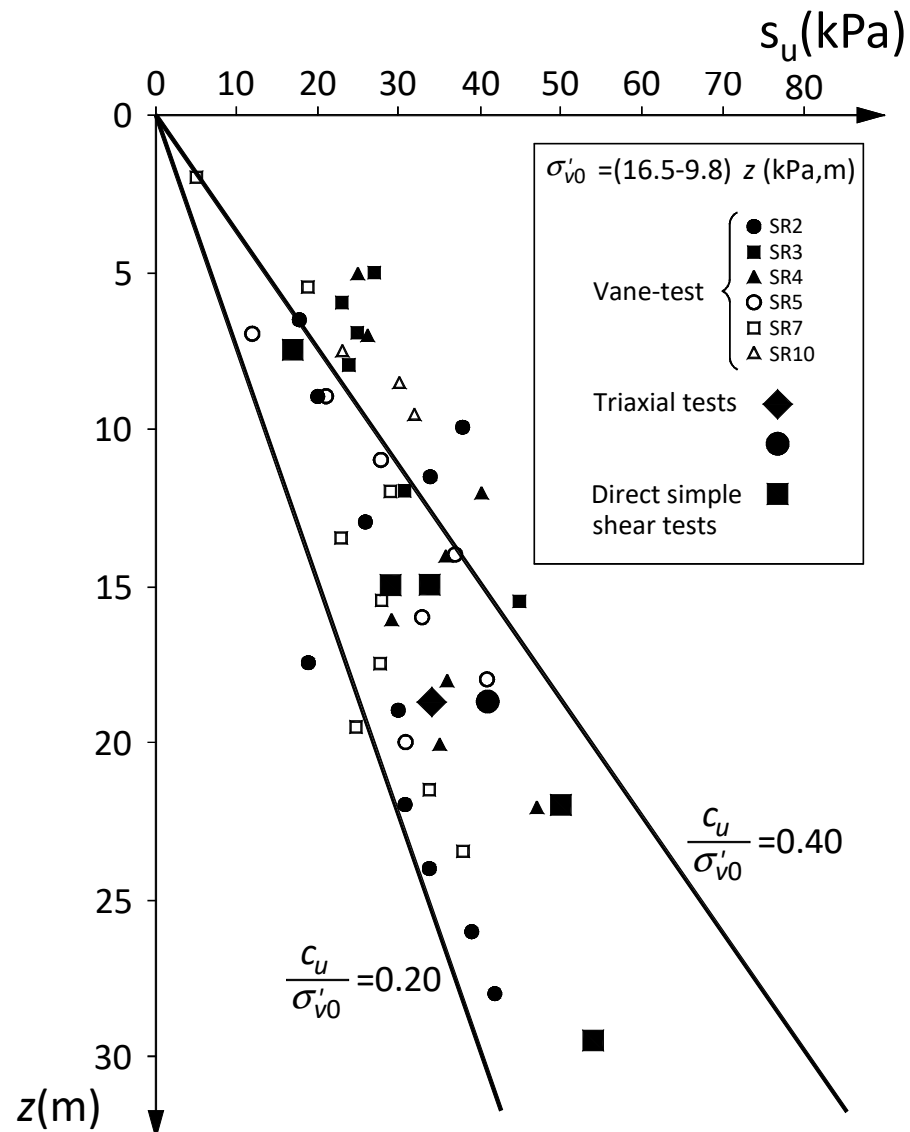
## OTHER POSSIBLE QUESTIONS (for the following weeks):

- For soil 3 (soft clay) depict the evolution in depth of the undrained shear strength  $s_u$  at the tidal flat and at the river bed.
- Assign a plausible value for  $s_u$  at the centre of the layer.

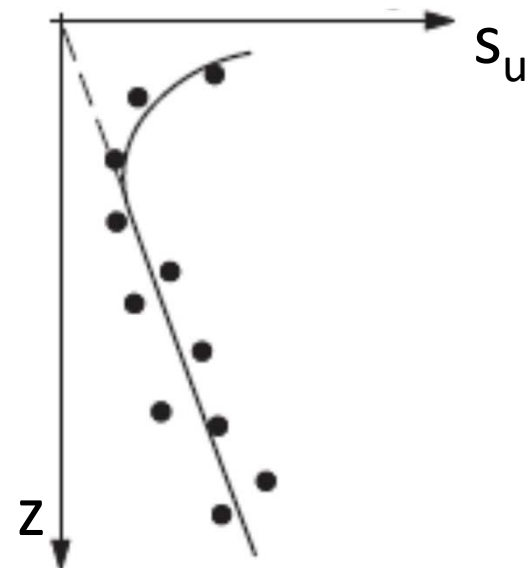
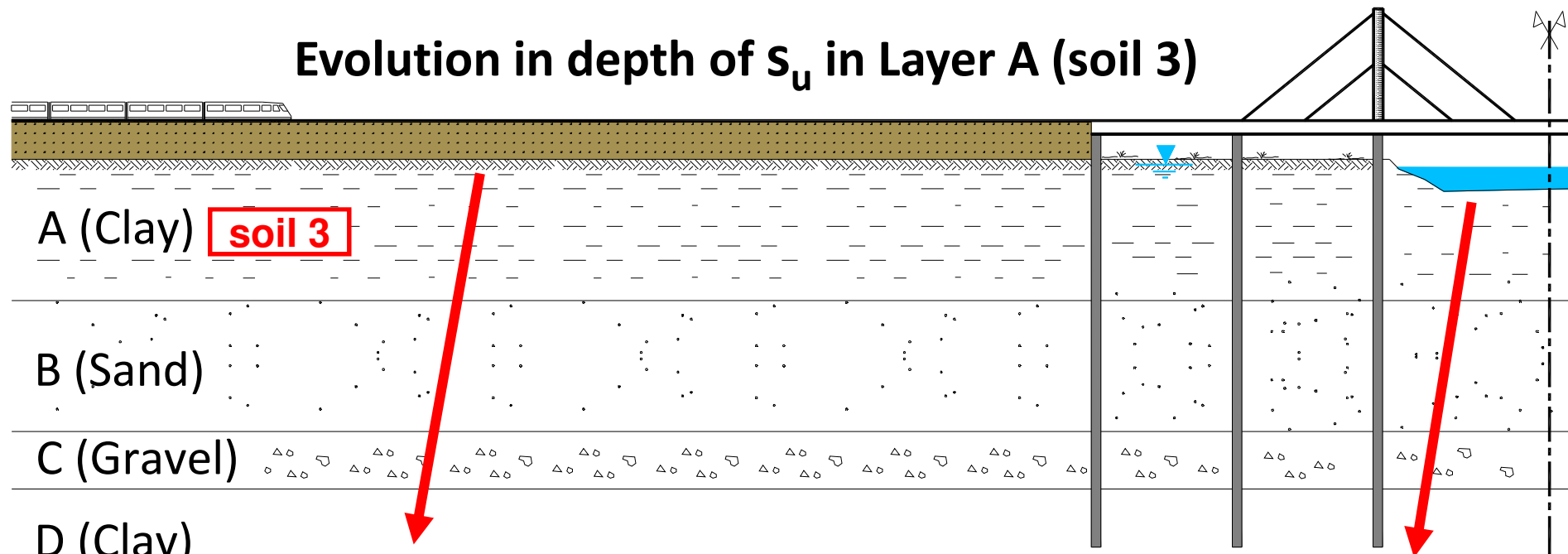


Soil	$w_L$ (%)	$w$ (%)	$w_p$ (%)	$e_{min}$	$e$	$e_{max}$	$I_c$	$I_D$ (%)
1	---	33	---	0.25	0.87	0.95	---	11
2	---	21	---	0.46	0.55	0.89	---	79
3	88	81	40	---	2.17	---	0.15	---
4	53	18	22	---	0.48	---	1.13	---

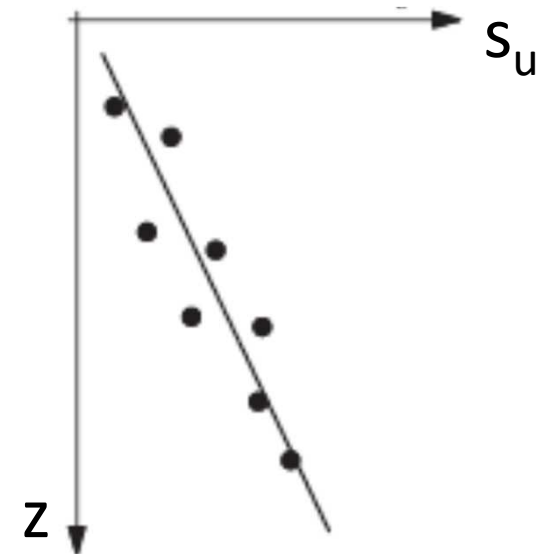
# Evolution of $s_u$ under the bed of river Tagus at the site of Vasco da Gama Bridge, Lisbon



## Evolution in depth of $s_u$ in Layer A (soil 3)

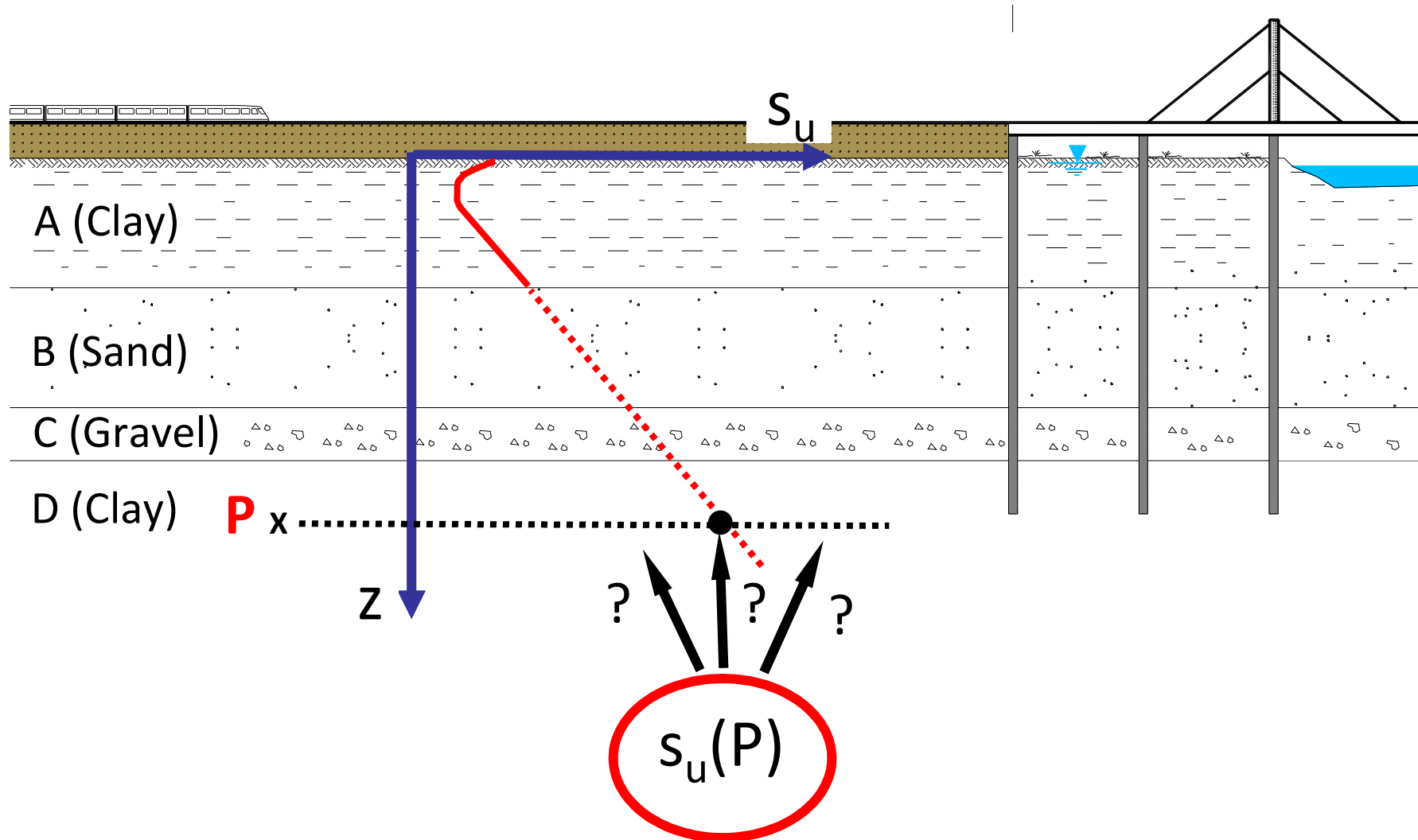


Tidal flat



River bed

- What would you say about the expected value of the undrained shear strength at point P in layer D, in comparison with the one obtained by simply extending the line drawn for layer A?



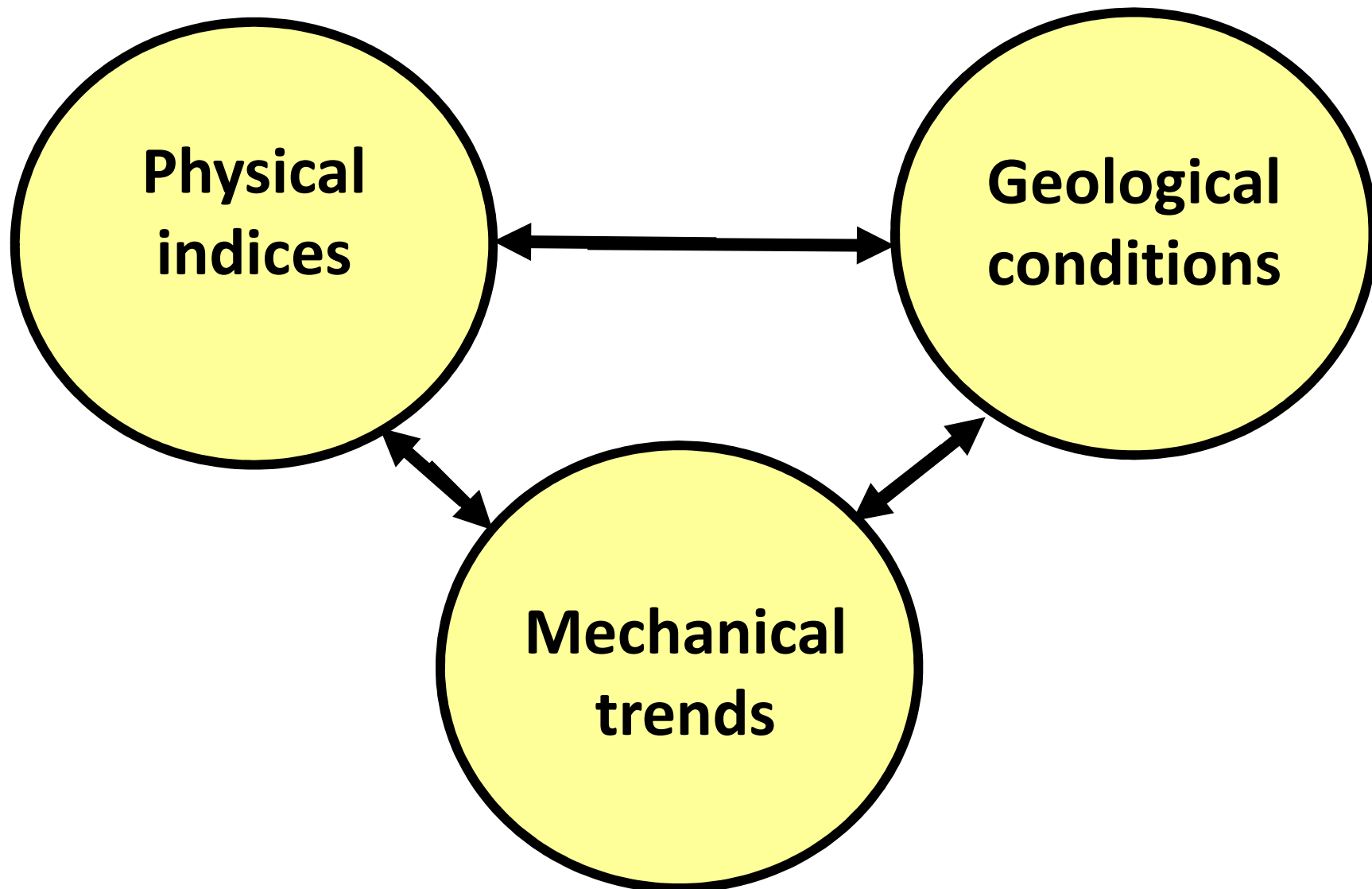
# CONCLUSIONS

In the presentation it was identified a *GAP* in the usual process of teaching/learning Soil Mechanics.

This *GAP* seriously affects the understanding that the mechanical behaviour – expressed by a series of abstract concepts – is totally controlled by the physical/geological soil characteristics...

... and these physical/geological characteristics are much easier to realize because they are intrinsically concrete!

**Then, the rational synthesis is not properly achieved.**





# CONCLUSIONS

Most of the main decisions of an experienced engineer are made on the basis of the interpretation of the site geology and of the physical/identification parameters of the relevant soil layers.

The characterization via mechanical lab and field tests and the calculations are essential in design but seldom lead to significant changes in the conception of the solution based on the aforementioned interpretation.

# CONCLUSIONS

The acquisition of expertise to assess “field atmosphere” usually requires years of experience but can be prepared at the University.

This requires training the ability to interpret the geological conditions and the physical-identification indices and to associate them to trends of the mechanical soil behaviour.

This training should begin even before studying the approaches that quantitatively characterize the mechanical soil behaviour. **But should continue and be improved in parallel with these approaches!!!**

# This strategy has many relevant advantages!

- Train the *eagle eye*: much can be extracted from the physical indices to assess the expected mechanical trends!
- Those simple but powerful ideas are easier to remain acquired in the future, as a *general knowledge*.
- They form an impressive *background* for the following (mechanical) chapters, whose subjects become more “realistic”.
- This is a good opportunity to introduce solutions to prevent undesirable soil behaviour (just the basic idea).
- This gives rise to very vivid classes, in which students gain enthusiasm because they discuss real engineering problems.

This is done in weeks 3 and 4 of the semester.

**Soil Mechanics** and **Introduction to Geotechnics** have been the two best rated disciplines by the students in the official educational surveys, over the last 20 years.



**Thank you for your attention!**



Photo by Francisco Piqueiro